



## **INTERIM PROJECT REPORT**

## Improving the Performance of Wall Furnaces in California

## Retrofit Wall Furnace Laboratory Test Report

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This is an interim report for CEC-PIR-18-005, "Improving the Performance of Wall Furnaces in California", a project designed to yield gas savings by replacing existing wall furnaces with more efficient retrofit models. This project gathers information about furnace performance, operation, emissions, and indoor air quality from laboratory testing and field monitoring of baseline and retrofit wall furnaces.

### Background

It is estimated that there are 1.4 million wall furnaces in California. Wall furnaces were introduced in California as early as 1930 and gained prevalence in single family homes and low-rise multifamily residential buildings as primary or auxiliary sources of heating. Not infrequently wall furnaces are as old as the buildings they occupy and may not have safety switches to prevent the furnaces from overheating. The oldest existing furnaces have rated thermal efficiencies of 50% while most standard replacement wall furnaces have rated thermal efficiencies of 70%.

More advanced wall furnaces achieve rated thermal efficiencies of 80% to 94% by eliminating pilot lights, using more efficient heat exchangers, and incorporating condensing or modulating technology. This means there is a substantial savings potential for a state-wide replacement program that promotes furnaces using these efficiency advancements.

This interim report documents laboratory test results for more efficient retrofit wall furnaces. Other interim reports for this project document field monitoring of these retrofit furnaces, and laboratory testing and field monitoring results of existing baseline furnaces.

## **Project Purpose and Approach**

The goal of this research is to demonstrate cost-effective solutions for retrofitting existing wall furnaces in California multifamily and single-family residences. This interim report gives the results of retrofit wall furnace laboratory testing to characterize the energy use, efficiency, and flue gas emissions of recently developed efficient wall furnaces. Other reports document results of field monitoring of these retrofit wall furnaces, and the laboratory testing and field monitoring results of existing baseline wall furnaces.

This project tested five retrofit wall furnaces which came directly from the manufacturer, Williams Comfort Products:

- One Williams 1753012 direct vent, fan-type, condensing wall furnace with a hot surface igniter and a two-stage heat exchanger, rated at 17,500 Btu/hr, 94% thermal efficiency, and 93% AFUE
- Two Williams AC2030TN top vent, fan-type, single-sided, low NOx wall furnace with an intermittent pilot, rated at 30,000 Btu/hr, 85% thermal efficiency, 82% AFUE
- One Williams AC3040TN top vent, fan-type, double-sided low NOx wall furnace with an intermittent pilot, rated at 40,000 Btu/hr, 83% thermal efficiency, 82% AFUE

• One Williams TG2030TN – top vent, fan-type, single-sided, low NOx wall furnace with an intermittent pilot, powered by a rechargeable battery, rated at 30,000 Btu/hr, 82% thermal efficiency, 80% AFUE.

### **Key Results**

Table 1 lists the rated and measured natural gas flows of each wall furnace, and their electrical power draw. All of these furnaces used more natural gas than their rated input, for an average 109% of rated input. None of these furnaces has a standing pilot, so their pilot gas use was zero. The Williams 1753012 condensing furnace used the most electricity during active heating and standby. The Williams AC2030TN furnaces drew about 12.5 watts only while active, and the AC3040TN furnace drew 12.5 watts all the time. The TG2030TN furnace was self-powered by a rechargeable battery, so did not draw any electrical power.

Wall Furnace Tested		Natural Gas Input				AC Power	
Model	Field Sites	Rated Btu/hr	Tested Btu/hr	% Rated Input	Pilot Btu/hr	Active W	Standby W
1753012 (condensing direct vent)	Hayward 3 & 4	17500	19 <mark>790</mark>	113%	0	100.1	0.0
AC2030TN #1 (single-sided low NOx)	LA 104-107	30000	34580	115%	0	12.5	0.0
AC2030TN #2 (single-sided low NOx)	LA 104-107	30000	31780	106%	0	12.6	0.1
AC3040TN (double-sided low NOx)	Oakland SFH	40000	41720	104%	0	12.4	0.0
TG2030TN (self-powered low NOx)	Sacto 4, 15 & 19	30000	31410	105%	0	0.0	0.0
	Average	29500	31856	109%	0	27.5	0.0

#### Table 1: Retrofit Wall Furnace Natural Gas Input and Electrical Power

Table 2 lists the rated and test-derived thermal efficiency and AFUE for each unit. All of these furnaces exceeded the 75% minimum thermal efficiency required by the American National Standards Institute regulations (ANSI Z21.86 2016) for fan-type wall furnaces. They also exceeded the minimum AFUE required by the Code of Federal Regulations (CFR 430.32 2022), 75% and 76% for furnaces below and above 42,000 Btu/hr rated input. However, all efficiencies derived from these laboratory tests were lower than their rated efficiencies, with thermal efficiency 3.8% lower and AFUE 3.1% lower on average.

Table 2: Retrofit Wall Furnace Thermal Efficiency and AFUE					
Wall Furnace Tested	Thermal	Efficiency	AF	UE	
				Rated	Т

			Lineericy	711 0 2		
				Rated	Tested	
Model	Field Sites	Rated TE	Tested TE	AFUE	AFUE	
1753012 (condensing direct vent)	Hayward 3 & 4	94%	89.5%	93%	88.0%	
AC2030TN #1 (single-sided low NOx)	LA 104-107	85%	81.8%	82%	80.4%	
AC2030TN #2 (single-sided low NOx)	LA 104-107	85%	81.2%	82%	79.9%	
AC3040TN (double-sided low NOx)	Oakland SFH	83%	79.0%	80%	77.8%	
TG2030TN (self-powered low NOx)	Sacramento 4, 15 & 19	82%	78.5%	80%	77.3%	
	Average Retrofit	87.0%	83.0%	85.2%	81.7%	

Table 3 lists preliminary energy use and emissions for each wall furnace. This is based on a typical day of operation as found during field testing of retrofit units, where the furnace cycles 1.0 times a day for 42 minutes per cycle and remains in standby for the rest of the day.

Wall Furnace Tested	Average Energy Use and Emission Rates					
				со	NOx	THC
Model	Field Sites	Btu/Day	kWh/Day	lbm/MMBtu	lbm/MMBtu	lbm/MMBtu
1753012 (condensing direct vent)	Hayward 3 & 4	13853	0.070	0.021	0.086	0.001
AC2030TN #1 (single-sided low NOx)	LA 104-107	24206	0.009	0.028	0.015	0.170
AC2030TN #2 (single-sided low NOx)	LA 104-107	22246	0.011	0.127	0.012	0.010
AC3040TN (double-sided low NOx)	Oakland SFH	29204	0.009	0.270	0. <mark>039</mark>	0.018
TG2030TN (self-powered low NOx)	Sacto 4, 19	21987	0.000	0.031	0.013	0.006
	Average	22299	0.020	0.096	0.033	0.041

Table 3: Retrofit Wall Furnace Energy Use and Emission Rates for aTypical Day of Operation

Not surprisingly, the largest capacity Williams AC3040TN furnace is estimated to use the most natural gas, and the smallest capacity Williams 1753012 furnace would use the least natural gas. The 1753012 furnace also uses the most electricity.

As for flue gas emissions:

- The Williams AC3040TN furnace had the highest CO emission rate due to relatively high CO emissions during steady state operation.
- The Williams 1753012 condensing furnace had the highest NOx emissions of these retrofit furnaces, due to high NOx emissions during steady state heating operation. The other three retrofit models were all low NOx furnaces, and substantial effort from the manufacturer appears to have gone into reducing their NOx emissions.
- The AC2030TN #1 furnace had a high total hydrocarbon emission rate, while the AC2030TN #2 furnace had low hydrocarbon emissions. The #1 furnace appears to have had a small natural gas leak which may be representative of leaks in actual installations.

There are no standards or regulations for emissions from wall furnaces. However, as detailed in Appendix A, the South Coast Air Quality Management District and the San Joaquin Valley Air Pollution Control District require central furnaces to keep nitrogen oxide emissions below 0.033 lbm/MMBtu. The AC2030TN and TG2030TN furnaces stay below this limit, while the AC3040TN furnace just exceeds the NOx limit. The 1753012 condensing furnace has an NOx emission rate that is 2.5 times the limit.

### **Knowledge Transfer and Next Steps**

The laboratory results documented in this study will be combined with results from the field monitoring to make more detailed estimates of the energy use and emissions of these retrofit wall furnaces. Similar laboratory testing and field monitoring will be done to characterize the performance of existing baseline wall furnaces. Baseline and retrofit data will then be used to estimate the energy savings and emission reduction potential of more efficient wall furnaces.

## Introduction

This project's overall objective is to characterize the operation, energy, indoor air quality, and emissions of existing and retrofit wall furnaces. The goal of this research is to investigate and demonstrate efficient solutions for retrofitting existing wall furnaces in California multifamily and single-family residences.

A wall furnace is a compact device installed within a home's wall cavity and used to heat a small number of rooms. Because they are less expensive, simpler to install, and take up less space than a central ducted furnace, they are commonly used in multifamily apartment complexes and smaller single-family homes.

Wall furnaces are categorized by how they distribute heat (gravity or fan-type), where their combustion air comes from (from inside for top vent furnaces, from outside for direct vent furnaces), how they ignite the burner (standing pilot, intermittent pilot, or hot surface igniter), and whether they use condensing technology. Additionally, furnaces can be either single-sided to serve just one room, or double-sided to serve rooms on either side of the wall in which it is installed. These wall furnace technologies are described in more depth in Appendix A.

Many California low-rise multifamily buildings and smaller homes use wall furnaces for space heating. Most of these existing wall furnaces are non-condensing gravity vented furnaces that use a standing pilot to ignite the burner. Wall furnaces are usually replaced only when the original unit is irreparably broken. Anecdotal information from Williams, the predominant wall furnace manufacturer, indicates that many older furnaces are still in operation, some without safety switches and with rated thermal efficiencies as low as 50%.

Most replacement wall furnaces are non-condensing gravity vented furnaces that just meet current efficiency standards. ANSI Z21.86 for Vented Gas-Fired Space Heating Appliances [ANSI Z21.96 2016] is the federal regulating standard for wall furnaces, It currently requires gravity wall furnace thermal efficiency to be at least 70% and fan-type wall furnace efficiency to be at least 75%. In addition, Annual Fuel Utilization Efficiency (AFUE) for wall furnaces are mandated under the Code of Federal Regulations [CFR Title 10 2022. (i) (1) and [CFR Title 10 2022. (i) (2)]. AFUE must be at least 65% to 76%, depending on furnace capacity and whether it is a gravity or fan-type wall furnace. More information about wall furnace efficiency standards is included in Appendix A.

Minimum wall furnace AFUE levels are well below the 81% AFUE requirement for standard central ducted furnaces and even further below the >90% AFUE that condensing furnaces can deliver. However, wall furnaces have recently been developed with thermal efficiencies as high as 85% and AFUE up to 82%, achieved by improving burners and removing standing pilot lights. In addition, condensing wall furnaces with thermal efficiency up to 94% and AFUE as high as 93% have been developed.

As with all primary gas space heating equipment in the state of California, emissions from wall furnace combustion are required to be vented to the outside to prevent the accumulation of indoor pollutants. There are no federal or California limits for wall furnaces regarding flue gas

emissions or indoor pollutants, although there are some limits on NOx emissions for natural gas-fired fan-type central furnaces in California's South Coast Air Quality Management District (SCAQMD) and the San Joaquin Valley Air Pollution Control District (SJVAPCD). See Appendix A for information about guidelines, standards, and regulations that pertain to indoor air quality and furnace emissions.

This project examines existing baseline and efficient retrofit wall furnaces in the laboratory and the field to assess their performance, ease of installation, operation, and reliability. Energy use, emissions, indoor air quality, and costs are assessed to help determine whether efficient retrofit wall furnace technologies should be promoted in California.

This project tested five retrofit wall furnaces which came directly from the manufacturer, Williams Comfort Products:

- One Williams 1753012 direct vent, fan-type, condensing wall furnace with a hot surface igniter and a two-stage heat exchanger, rated at 17,500 Btu/hr, 94% thermal efficiency, and 93% AFUE
- Two Williams AC2030TN top vent, fan-type, single-sided, low NOx wall furnace with an intermittent pilot, rated at 30,000 Btu/hr, 85% thermal efficiency, 82% AFUE
- One Williams AC3040TN top vent, fan-type, double-sided low NOx wall furnace with an intermittent pilot, rated at 40,000 Btu/hr, 83% thermal efficiency, 82% AFUE
- One Williams TG2030TN top vent, fan-type, single-sided, low NOx wall furnace with an intermittent pilot, powered by a rechargeable battery, rated at 30,000 Btu/hr, 82% thermal efficiency, 80% AFUE.

Laboratory testing involved running the furnaces through a protocol that included standby, startup, steady state, and shutdown operation while measuring:

- Inlet, outlet, and exhaust temperatures of the wall furnaces
- Carbon monoxide, nitrogen oxide, and total hydrocarbon flue gas emissions
- Natural gas flow rates

In other project work, these test results will be applied to field monitoring data for these furnaces to estimate their energy use and emissions. Existing baseline furnaces will also be laboratory tested and field monitored as part of this project. Comparisons of baseline and retrofit energy use and emissions will be made to evaluate the savings that can be realized through the installation of more efficient retrofit furnaces.

Laboratory testing was conducted within the Residential and Commercial Equipment laboratory on the Des Plaines, IL GTI Energy campus. Wall furnace tests included measurement of intake, burner and exhaust temperatures, natural gas, electricity, and exhaust gas emission levels.

### **Furnaces Tested**

This project tested a total of five retrofit wall furnaces which came directly from the manufacturer, Williams Comfort Products. The characteristics of each retrofit furnace are presented in Table 1. Additional furnace samples were also installed for monitoring at field sites (see Retrofit Wall Furnace Field Monitoring Report).

Field Sites	Manufacturer	Model	Input Btu/hr	Thermal Efficiency	Rated AFUE	Features
Hayward 3 & 4	Williams	1753012	17,500	94%	93%	<ul> <li>Direct Vent</li> <li>Condensing</li> <li>Hot Surface Igniter</li> <li>2 Stage Heat Exchanger</li> <li>Fan-Type w/AC Power</li> </ul>
Los Angeles 104-107	Williams	AC2030TN #1 & #2	30,000	85%	82%	<ul> <li>Top Vent</li> <li>Intermittent Pilot</li> <li>Fan-Type w/AC Power</li> <li>Low NOx emissions</li> <li>Single-Sided</li> <li>Traditional Form Factor</li> </ul>
Oakland SFH	Williams	AC3040TN	40,000	83%	80%	<ul> <li>Top Vent</li> <li>Intermittent Pilot</li> <li>Fan-Type w/AC Power</li> <li>Low NOx emissions</li> <li>Double-Sided</li> <li>Traditional Form Factor</li> </ul>
Sacra- mento 4, 15 & 19	Williams	TG2030TN	30,000	82%	80%	<ul> <li>Top Vent</li> <li>Intermittent Pilot</li> <li>Fan-Type w/Battery</li> <li>Low NOx emissions</li> <li>Traditional Form Factor</li> </ul>

 Table 1: Laboratory Tested Retrofit Wall Furnace Characteristics

The Williams AC2030TN, AC3040TN, and TG2030TN furnaces shown in Figure 1 are all top vent furnaces with traditional form factors. These furnaces are drop-in replacements for older wall furnaces and are usually installed on inside walls. They draw combustion air from the indoors then vent it through a vertical flue to the roof. They are also all "low NOx" furnaces, which means their combustion is carefully controlled to reduce nitrogen oxides emissions.

# Figure 1: High Efficiency Williams Wall Furnaces Tested in this Project from left to right: 1753012, AC2030TN, AC3040TN, TG2030TN



The AC2030TN and AC3040TN furnaces must also be connected single-phase AC power to run their fans. The TG2030TN furnace is self-powered and uses a rechargeable battery to operate the fans.

The Williams 1753012 furnace, shown on the left of Figure 1, is a direct vent condensing furnace with a different form factor than the typical tall, skinny wall furnaces. It is usually installed in an outside wall for easier access to outside air for combustion, but can be installed on an inside wall if the appropriate ducting to the outside is used. It must also have access to a drain through which to channel condensate water. This furnace must also be connected to single-phase AC power to operate its fan. Note that although this condensing furnace is very efficient, it is not a "low NOx" furnace like the other retrofit furnaces being tested, so it is expected it will have higher nitrogen oxides emissions than the rest of the retrofit furnaces.

Laboratory testing included measurement of furnace natural gas flow, electricity use, operating temperatures, and concentrations of carbon monoxide (CO), nitrogen oxides (NOx), and total hydrocarbons (THC) in exhaust gases. The testing protocol covered furnace operation during standby, startup, steady state, and shutdown. Parameters derived from measurements include each furnace's input capacity and pilot gas use, efficiency, and pollutant emission rates

### **Measurements and Test Equipment**

The following table details the measurement equipment used in the laboratory.

Measurement	Description	Range, Accuracy
Flow-Field Temperatures	1/8" J-type exposed bead thermocouple	32-1328ºF/0-750ºC, ±2.2ºC
Ambient Temperature	1/8" J-type exposed bead thermocouple	32-1328ºF/0-750ºC, ±2.2ºC
Ambient Humidity	Omega OM-HL-SH-EX	0-100%RH, ±5%RH
Data Acquisition Modules	National Instruments CompactDAQ	-
Stack O <sub>2</sub>	Horiba PG350	Span 25% O <sub>2</sub> , ±1%
Stack CO <sub>2</sub>	Horiba PG350	Span 25% CO <sub>2</sub> , ±1%
Stack NO <sub>x</sub>	Horiba PG350	Span 100 ppm, , ±1%
Stack CO	Horiba PG350	Span 500 ppm, ±1%
Stack THC	Rosemount Analytical 400A	Span 1000 ppm, 0.5ppm
Gas Flow Rate	American Meter AC250	8 pulses/ft <sup>3</sup>

Table 4:	Laboratory	Test I	Equipment

While the furnaces were not installed into a wall assembly designed to mimic a typical internal wall cavity, GTI Energy's Des Plaines laboratory technicians followed all other ANSI Z21.86 test protocols for measurement of temperatures, exhaust gas emissions, and natural gas flow.

Inlet temperatures were measured using a thermocouple in the center of the furnace inlet grill at the bottom of each furnace.

Exhaust air temperatures were measured approximately three inches from the combustion air outlet using a probe inserted into the exhaust air duct, with three thermocouples to measure temperatures across the duct span.

Burner outlet temperature measurements were recorded using an array of nine equally spaced thermocouples, following the dimensions outlined in section 11.6.1 of ANSI Z21.86 (ANSI Z21.86 2016) to ensure an average reading in the case of a heterogeneous flow field. The burner thermocouple array was attached to the center of the burner outlet to measure temperatures of the heated air leaving the furnace.

A continuous measurement of exhaust constituents, including oxygen (O<sub>2</sub>), carbon dioxide (CO<sub>2</sub>) carbon monoxide (CO), nitrogen oxides (NO<sub>x</sub>), and unburned total hydrocarbons (THC) were measured and reported on a dry basis. Emission measurements were made through a system of three 0.25-inch stainless steel inserts in a manifold arrangement in the stack downstream of the flue temperature and pressure measurements. The emission sample points were arranged to account for exhaust streams that are non-homogenous. Combustion

products were drawn through a vacuum pump and passed through a series of desiccants to provide a dry sample to a bank of analyzers located within the laboratory. Each analyzer was calibrated before each test run against a "zero" gas of pure nitrogen and then against a span gas measured in an independent analyzer.

GTI's laboratory measures the composition of the natural gas used for testing every two weeks. Samples of the natural gas being used for combustion are analyzed through a calorimeter. Although variations in gas characteristics tend to be small, the latest available house gas data was used for analysis of each tested wall furnace.

Natural gas for all wall furnace tests was delivered at a pressure of 6.8 inches water column, at the high end of the recommended 5 to 7 inches water column range for each furnace.

### **Test Procedure**

The following operating procedure was followed for wall furnace tests:

- Start up all test measurement equipment
- Calibrate all sensors following equipment manufacturer procedures
- Adjust gas supply pressure to 6.8 inches water column
- Begin recording measurements
- Light furnace pilot
- Leave furnace on standby with the pilot lit for 30 minutes to record any pilot and/or electrical energy use
- Cold start start up furnace and allow it to run for 45 minutes (steady state operation from cold start is usually reached in less than 30 minutes)
- Turn off furnace and let it sit in standby with the pilot lit for 1.5 minutes
- Hot start start up furnace again and let it run for 30 minutes (steady state operation from a hot start is usually reached in less than 20 minutes)
- Turn off furnace and leave on standby with pilot lit for 15 minutes
- End test

This entire procedure took about two hours and allowed for the measurement of the furnace in standby, startup, steady state, and shutdown operating modes. For retrofit furnaces without pilot lights, standby operating times at the beginning and end of the test were reduced since this time was not needed to measure pilot light natural gas use.

Some problems were encountered on three retrofit furnaces when following this procedure:

- The double-sided Williams AC3040TN furnace shut itself off after reaching steady state during the cold start portion of the test
- Both the Williams AC2030TN furnaces were difficult to restart on the hot start portion of the test, with one shutting off after the first restart and needing to be started again

Despite these problems, which were adjusted for during post-processing of the test data, all the pertinent information was captured for all furnaces.

## **Data Corrections**

The gas analyzer and burner data acquisition system are separate pieces of equipment operating on slightly different time stamps. In addition, the flow of exhaust gases to the analyzer added a time delay. Data from the gas analyzer was synchronized with burner temperatures by lining up changes in  $O_2$  and  $CO_2$  concentrations with exhaust temperature changes over time.

The following corrections were made to the collected data:

- $O_2$  concentration maximum was adjusted to 20.9%, down from as much as 21.3% within +/- 1% measurement accuracy
- CO<sub>2</sub> concentration was adjusted to match the corrected O2 concentration during combustion based on the house natural gas characteristics
- CO and NOx minimum concentrations were adjusted to 0.0% (up from -0.13 ppm which is within +/- 1% measurement accuracy)

CO, NOx, and THC concentrations are reported as absolute values, and not corrected to a standard  $O_2$ % concentration as is sometimes done with furnace and boiler emissions. While the retrofit furnaces all ran with an exhaust gas  $O_2$ % of about 14%,  $O_2$ % varied from 10% to 19% for the baseline furnaces due to their no longer being well-tuned. To report actual emissions from these furnaces in their existing condition, emission concentrations were not standardized.

## **Analysis of Test Data**

The fuel input capacity of the pilot light and during active combustion is operating was calculated from the measured gas flow rate as follows:

Qin = Fuel input capacity  $Btu/hr = 60 \times Active Gas$  Flow Rate x Heating Value/Timestep

Qp= Pilot Btu/hr = 60 x Standby Gas Flow Rate x Heating Value / Timestep

Active Gas Flow Rate,  $ft^3$  = measured value during active combustion

Standby Gas Flow Rate,  $ft^3$  = measured during standby conditions

Heating value,  $Btu/ft^3$  = from house natural gas used during testing

Timestep = time between measurements in minutes

Emission mass flow rates are normalized to the gas input rate from their absolute measured concentrations as follows:

#### **Equation 1. Converting Emission Concentration to Emission Rate**

Emission Rate, Ibm/MMBtu =  $\frac{\text{Concentration x Molecular Weight x Fd x 20.9}}{(20.9 - O_2\%) \text{ x Molar Volume}}$ 

Concentration, ppm = absolute measured pollutant concentration

Molecular weight, lbm/lbmole = 28.0097 for CO, 46.0047 for NOx as NO2, and 16.04206 for Total Hydrocarbons (THC) as methane

- Fd, lbm/MMBtu = 10<sup>6</sup> x (3.64 x %H + 1.53 x %C + 0.57 x %S + 0.14 x %N 0.46 x %O)/HHV, using dry weight percentages of each element in the house natural gas used for testing
- $O_2\%$  = adjusted oxygen percentage in exhaust stream

HHV, Btu/lbm = higher heating value of house natural gas used for testing

Molar Volume, dry ft<sup>3</sup>/lbmole = 385.3 at 68°F and 1 atmosphere

Estimated test thermal efficiency and AFUE are calculated for steady state operation based on Title 10 of the Code of Federal Regulations, Appendix O, Subpart B, Part 430 (CFR 430.32 2022), using the following equations:

Test  $\eta_{SS-WT}$  automatic = 100 - Ls ss - L la

Test  $\eta_{SS-WT}$  manual =  $\eta_{SS-WT}$  – L i on

Overall Test  $\eta_{SS-WT} = (\eta_{SS-WT} \text{ automatic} + \eta_{SS-WT} \text{ manual}) / 2$ 

Test AFUE automatic =  $[0.968 \text{ x} \eta_{SS-WT}] - 1.78D_f - 1.89D_s - 129P_f - 2.8L_I + 1.81$ 

Test AFUE manual = [ 2950 x  $\eta_{ss-wt}$  x  $\eta_{part load}$  x Qin] / [2950 x Qin + 2.083 x 4600 x  $\eta_{part load}$  x Qp]

Overall Test AFUE = (Test AFUE automatic + Test AFUE manual) / 2

 $\eta_{SS-WT}$  = weighted-average steady state efficiency =  $100 - L_{L,A} - L_{s,SS}$ 

 $L_{L,A}$  = latent heat loss = 9.55 for natural gas fueled furnaces

 $L_{S,SS}$  = sensible heat loss at steady state =  $C(R_{T,S} + D)(T_{S,SS} - T_{RA})$ where C = 0.0175, D = 0.171

 $R_{T,S}$  = actual to stoichiometric air mass flow rate = A + B/X<sub>co2</sub> where A = 0.0919, B = 10.96, and X<sub>co2</sub> is the concentration of carbon dioxide present in dry stack gas

 $T_{S,SS}$  =steady state flue gas temperature

 $T_{RA}$  = ambient room temperature

 $D_{f}$  = off-cycle flue gas factor = 1 for atmospheric burner type furnaces

 $D_s$  = off-cycle stack gas factor and is equal to zero for direct vent furnaces

 $P_f$  = pilot fraction =  $Q_p/Q_{in}$ 

 $L_j$  = jacket loss for floor furnaces, which is zero in this study

 $\eta_{part \ load}$  = part load utilization efficiency =  $\eta_{SS-WT} - L_{I \ ON}$ 

 $L_{\rm i\,ON}$  = on cycle infiltration heat loss = (70-45) x (100 x Cp x S/F) x (1+ Rts x (A/F) / HHV

Cp = specific heat of air, 0.24 Btu/lbm R

S/F =stack/mass flow ratio = 1.0

A/F = stoichiometric air-fuel ratio = 14.45 for natural gas

Note that the test apparatus was not installed in a fabricated wall assembly as designated in ANSI Z21.86 2016, therefore this report's efficiencies are not official rating tests and are for informational and comparative purposes only.

Unlike central furnaces which are most often allowed to cycle automatically to meet a thermostat setting, wall furnaces are much more likely to be turned on and off manually when occupants want heating. To reflect this operation, thermal efficiency and AFUE were found as the average of the efficiency for heaters that are automatically controlled and the efficiency for heaters with manual controls.

Laboratory test results are presented here for each retrofit wall furnace. Data for each furnace is presented in standardized plots that show their operation during testing. Two pages of test result plots are shown for each of the five retrofit furnaces:

- Cold start operation including five minutes of standby operation beforehand
- Hot start operation plus a summary of steady state conditions

Each page of test results includes the following information:

- Time to reach steady state and measured values at time intervals of 0%, 20%, 40%, 60%, 80% and 100% of steady state for the cold start, and values at time intervals of 0%, 33%, 67%, and 100% of steady state time for the hot start
- Fuel use, including both natural gas use and electrical power draw
- Exhaust, burner, inlet, and room temperatures
- Exhaust gas concentrations including O2%, CO2%, and CO, NOx, and THC concentrations in parts per million
- Note that vertical scales vary on emissions plots to show their values more clearly



#### Figure 2: Williams 1753012 (Hayward 3 & 4), Cold Start



#### Figure 3: Williams 1753012 (Hayward 3 & 4), Hot Start & Steady State



#### Figure 4: Williams AC2030TN #1 (Los Angeles 104-107), Cold Start



#### Figure 5: Williams AC2030TN #1 (Los Angeles 104-107), Hot Start & Steady state



#### Figure 6: Williams AC2030TN #2 (Los Angeles 104-107), Cold Start



#### Figure 7: Williams AC2030TN #2 (Los Angeles 104-107), Hot Start & Steady State



#### Figure 8: Williams AC3040TN (Oakland SFH), Cold Start



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#### Figure 11: Williams TG2030TN (Sacramento 4, 15 & 19), Hot Start & Steady State

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Below laboratory test results for all five tested retrofit wall furnaces are compared, including their fuel use, electricity use, combustion and thermal characteristics, efficiency, and emissions.

## **Retrofit Wall Furnace Fuel Use**

Table 5 lists the measured fuel input for all tested wall furnaces, including natural gas use during heating and electrical power draw during active heating and standby periods. Note that a gas pressure of 6.8 inches water column was used during all testing, at the high end of the recommended 5 to 7 inches water column range for each furnace.

Wall Furnace Tested		Natural Gas Input				AC Power	
		Rated	Tested	% Rated	Pilot	Active	Standby
Model	Field Sites	Btu/hr	Btu/hr	Input	Btu/hr	W	W
1753012 (condensing direct vent)	Hayward 3 & 4	17500	19790	113%	0	100.1	0.0
AC2030TN #1 (single-sided low NOx)	LA 104-107	30000	34580	115%	0	12.5	0.0
AC2030TN #2 (single-sided low NOx)	LA 104-107	30000	31780	106%	0	12.6	0.1
AC3040TN (double-sided low NOx)	Oakland SFH	40000	41720	104%	0	12.4	0.0
TG2030TN (self-powered low NOx)	Sacto 4, 15 & 19	30000	31410	105%	0	0.0	0.0
	Average	29500	31856	109%	0	27.5	0.0

Table 5: Retrofit Wall Furnace Natural Gas Input and Electrical Power

All the retrofit furnaces used more natural gas than their rated value, from 4 to 15% more, and 9% more on average. It is not clear why test capacity was higher than rated capacity, since these tests used the same gas pressure as is used to derive rated capacity. None of these furnaces had standing pilots, so they used no pilot energy use when in standby mode.

Both tested AC2030TN furnaces drew about 12.5 W of power when active to run their fans, but that power draw dropped to essentially zero when in standby mode. The double-sided AC3040TN furnaces also used about 12.5 W of power when active, but also drew 12.5 W when in standby. The 1753012 direct vent condensing furnace drew the largest amount of power, using 100 W both while actively firing and in standby. Subsequent field monitoring of the AC3040TN and 1753012 furnaces found their power draw dropped to zero when in standby, so standby power draw in Table 5 was adjusted to zero for these furnaces. The TG2030TN furnace didn't draw any electrical power, as it's powered by a rechargeable battery.

## **Retrofit Wall Furnace Combustion and Thermal Characteristics**

Table 6 lists the percentages of oxygen and carbon dioxide found in the exhaust gases of each wall furnace, which is an indicator of combustion efficiency. Oxygen levels around 14% and carbon dioxide around 4% indicate that the fuel-air ratio is neither too rich nor too lean for good combustion. All the retrofit furnaces have flue gas oxygen levels that indicate adequate fuel-air ratio for good combustion. There are variations of about 1% in O2 and 0.7% in CO2

between the furnaces, most likely because of differences in how manufacturers decided to operate each furnace to achieve both high efficiency and low NOx emissions.

Wall Furnace Tested	Combustion		
Model	Field Sites	% 02	% CO2
1753012 (condensing direct vent)	Hayward 3 & 4	13.0	4.5
AC2030TN #1 (single-sided low NOx)	LA 104-107	14.1	3.8
AC2030TN #2 (single-sided low NOx)	LA 104-107	14.0	3.8
AC3040TN (double-sided low NOx)	Oakland SFH	13.2	4.5
TG2030TN (self-powered low NOx)	Sacto 4, 19	13.6	4.1
	Average	13.6	4.2

#### Table 6: Combustion Exhaust Gas Oxygen and Carbon Dioxide Percentages

Table 7 lists the time to reach steady state conditions during cold and hot starts for each tested furnace. Steady state conditions were assumed to be reached when the average exhaust temperature first rose to within 3°F of the maximum temperature achieved during each respective cold or hot start.

Wall Furnace Tested		Startup		Avg Hot & Cold Start Steady State Conditions			
Model	Field Sites	Cold Start	Hot Start	Exhaust °F	Burner °F	Inlet °F	Room °F
1753012 (condensing direct vent)	Hayward 3 & 4	23.6	10.0	83.7	162.6	79.0	74.5
AC2030TN #1 (single-sided low NOx)	LA 104-107	37.7	14.2	218.2	152. <mark>4</mark>	91.4	76.0
AC2030TN #2 (single-sided low NOx)	LA 104-107	32.7	25.5	232.9	<b>144</b> .0	85.5	76.5
AC3040TN (double-sided low NOx)	Oakland SFH	23.6	8.4	299.8	235.0	75.0	75.0
TG2030TN (self-powered low NOx) Sacramento 4, 15 & 19		38.0	16.4	289.4	154.6	82.8	74.2
Average Retrofit		31.1	<b>1</b> 4.9	<b>22</b> 4.8	169.7	82.7	75.2

#### Table 7: Retrofit Wall Furnace Steady State Conditions, deg F

Steady state was reached within 23 to 38 minutes during cold starts, and within 8 to 16 minutes during hot starts. In all furnaces it took longer to reach steady state in cold starts.

Table 7 also lists the average cold and hot start steady state exhaust, burner, inlet, and room temperatures reached for each furnace. Room temperatures varied since the test facility was not isolated in a climate-controlled room. Inlet temperatures to each furnace tended to be higher than the room temperature, indicating that the furnaces entrain some of the heat they produce directly back into the unit. This entrainment may have been affected by a lack of conditioning and air circulation in the test facility.

Average exhaust temperatures in the non-condensing furnaces vary by more than 200°F, from around 220°F on the AC2030TN furnace to around 290°F on the AC3040TN and TG2030TN furnaces. Presumably exhaust temperature differences are a consequence of the adjustments made to fuel-air ratios to control nitrogen oxides emissions for these low NOx furnaces. The exhaust temperature for the condensing furnace was much lower, at about 85°F, which is expected because a heat exchanger is used to recover heat from the exhaust air. This heat recovery is what makes the condensing furnace so efficient.

## **Retrofit Wall Furnace Efficiency**

Table 8 lists the rated and tested thermal efficiency and Annual Fuel Utilization Efficiency (AFUE) of each wall furnace. Note that these are not official rated values since the furnaces were not installed into a fabricated wall cavity assembly as specified by the ANSI Z21.86 2016 test standard.

Wall Furnace Tested		Thermal	Efficiency	AFUE	
		Rated	Tested	Rated	Tested
Model	Field Sites	TE	TE	AFUE	AFUE
1753012 (condensing direct vent)	Hayward 3 & 4	94%	89.5%	93%	88.0%
AC2030TN #1 (single-sided low NOx)	LA 104-107	85%	81.8%	82%	80.4%
AC2030TN #2 (single-sided low NOx)	LA 104-107	85%	81.2%	82%	79.9%
AC3040TN (double-sided low NOx)	Oakland SFH	83%	79.0%	80%	77.8%
TG2030TN (self-powered low NOx)	Sacramento 4, 15 & 19	82%	78.5%	80%	77.3%
Average Retrofit		87.0%	83.0%	85.2%	81.7%

#### **Table 8: Retrofit Wall Furnace Tested Thermal Efficiency and AFUE**

Tested values of thermal efficiency on all furnaces were 3.2% to 4.5% lower than their rated thermal efficiencies, and 3.8% lower on average. Tested AFUE values were 1.6% to 5.0% lower than rated AFUE values, and 3.1% lower on average. The two AC2030TN furnaces gave similar thermal efficiency and AFUE results.

Recall that the furnaces were not installed in fabricated wall assemblies during this laboratory testing This may have allowed more heat loss from back side of the furnaces than they would see during official rating tests, thereby lowering the test efficiency. The thermal efficiencies and AFUE values from this report's testing should therefore be used only for comparative purposes between furnaces.

According to ANSI Z21.86-2016 as listed in Table 13 of Appendix A, the minimum thermal efficiency for fan-type furnaces should be 75%. All retrofit furnaces still tested well above that minimum, even if they tested short of their ratings.

As listed in Table 14 of Appendix A, the minimum AFUE from the Code of Federal Regulations for fan-type wall furnaces is 75% for furnaces below 42,000 Btu/hr and 76% for furnaces above 42,000 Btu/hr. All tested furnaces exceeded these minimum standards, even though these test results fell short of their rated AFUE values.

## **Retrofit Wall Furnace Emissions**

Emission concentrations for each wall furnace were measured using a gas analyzer probe inserted in the exhaust stream. Emissions were then averaged over four operating conditions:

- Pilot while in standby with only the pilot light burning natural gas
- Startup from the start of combustion until the average exhaust temperature reaches steady state as defined by heating up to within 2°F of the maximum temperature achieved during that test

- Steady State after the exhaust temperature reaches steady state and before the burner shuts off
- Shutdown for 1.5 minutes after gas flow to the burner is turned off and only the pilot light burning natural gas

Exhaust stream concentrations in parts per million are converted to emission mass flow rates in lbm per MMBtu using Equation 1. Note that this conversion uses the percentage of oxygen in the exhaust flow to account for the fuel input, not the measured natural gas flow itself. There are often brief high concentrations and mass flow rates of pollutants in the exhaust stream at startup and shutdown. These spikes get ameliorated somewhat because startup emissions get folded into the entire startup time to steady state, and because shutdown emissions are assumed to occur at the much lower pilot gas rate.

Table 9, Table 10, and Table 11 list the carbon monoxide, nitrogen oxides, and total hydrocarbon emission rates found during testing of each wall furnace.

Wall Furnace Tested		Carbon Monoxide, lbm/MMBtu			
Model	Field Sites	Standby	Startup	Steady State	Shutdown
1753012 (condensing direct vent)	Hayward 3 & 4	1.093	0.027	0.017	0.023
AC2030TN #1 (single-sided low NOx)	LA 104-107	0.620	0.045	0.001	3.106
AC2030TN #2 (single-sided low NOx)	LA 104-107	2.216	0.183	0.002	0.681
AC3040TN (double-sided low NOx)	Oakland SFH	0.230	0.145	0.348	0.048
TG2030TN (self-powered low NOx)	Sacto 4, 19	0.075	0.042	0.012	0.041
	Average	0.846	0.088	0.076	0.780

#### Table 9: Baseline Wall Furnace Carbon Monoxide Emissions

#### Table 10: Baseline Wall Furnace Nitrogen Oxides Emissions

Wall Furnace Tested		Nitrogen Oxides, Ibm/MMBtu			
Model	Field Sites	Standby	Startun	Steady State	Shutdown
1753012 (condensing direct vent)	Hayward 3 & 4	0.178	0.083	0.089	0.266
AC2030TN #1 (single-sided low NOx)	LA 104-107	0.027	0.018	0.012	0.019
AC2030TN #2 (single-sided low NOx)	LA 104-107	0.030	0.012	0.012	0.015
AC3040TN (double-sided low NOx)	Oakland SFH	0.077	0.032	0.043	0.032
TG2030TN (self-powered low NOx)	Sacto 4, 19	0.039	0.014	0.013	0.016
	Average	0.070	0.031	0.034	0.069

#### **Table 11: Baseline Wall Furnaces Total Hydrocarbon Emissions**

Wall Furnace Tested		Total Hydrocarbons, lbm/MMBtu				
Model	Field Sites	Standby	Startup	Steady State	Shutdown	
1753012 (condensing direct vent)	Hayward 3 & 4	0.004	0.003	0.000	0.000	
AC2030TN #1 (single-sided low NOx)	LA 104-107	0.171	0.160	0.258	1.499	
AC2030TN #2 (single-sided low NOx)	LA 104-107	0.008	0.013	0.000	0.597	
AC3040TN (double-sided low NOx)	Oakland SFH	0.004	0.013	0.026	1.386	
TG2030TN (self-powered low NOx)	Sacto 4, 19	0.002	0.004	0.032	1.144	
	Average	0.038	0.038	0.063	0.925	

As was seen in the plots of emission concentrations over time during the baseline wall furnace tests, carbon monoxide and total hydrocarbon emission rates tend to be higher during startup and especially shutdown, when combustion is not quite complete. In standard wall furnaces without control of excess air during combustion, nitrogen oxide emissions tend to be higher while heating is actively operating due to poor fuel-air ratios. However, furnaces with good combustion controls like most of these retrofit furnaces have much lower steady state nitrogen oxides emission rates.

There are some clear outliers with high emission rates:

- Both AC2030TN furnaces have high CO emission rates at startup and shutdown, and the 1753012 furnace has a high CO emission rate at startup, while the AC3040TN furnace had higher CO emission rates during steady state operation
- Nitrogen oxides emission rates for the four non-condensing furnaces are quite low, while the 1753012 condensing furnace has much a higher NOx emission rate
- All four non-condensing furnaces have high total hydrocarbon emission rates at shutdown, and the AC2030TN #1 has high hydrocarbon emission rates across the board

Although the two theoretically identical AC2030TN furnaces had similar thermal efficiency and AFUE, their emissions profiles were somewhat different from each other. Nitrogen oxides emissions were similar on both furnaces, but carbon monoxide and hydrocarbon emissions varied. CO emissions were high on both furnaces when not in steady-state, but were higher during shutdown on #1 and during standby and startup on #2. Hydrocarbon emissions were high during all operating modes on #1 and high at shutdown on #2. This indicates that both furnaces had poor fuel-air mixing as their gas valve opens and closes, and AC2030TN #1 may have had a small natural gas leak.

There are no standards or regulations for emissions from wall furnaces. However, as detailed in Appendix A: Wall Furnace Characteristics, the South Coast Air Quality Management District and the San Joaquin Valley Air Pollution Control District require central furnaces to keep nitrogen oxide emissions below 0.033 lbm/MMBtu.

From Table 10, it is seen that the two AC2030TN furnaces stay below the NOx limit for central furnaces. The AC3040TN and TG2030TN furnaces exceed the 0.033 lbm/MMBtu NOx limit in at least one of their operating modes. The 1753012 condensing furnace's NOx emission rates were at least 2.5 times the limit in all operating modes.

## Wall Furnace Energy Use and Emissions during Typical Operation

To investigate energy use and emissions further, Table 12 lists preliminary estimates of fuel use and emission rates over a typical day of operation for each retrofit furnace. Field testing showed that the average retrofit furnace was operated for an average of 1.0 on-off cycles every day for 42 minutes per cycle. Natural gas use, electricity use, and flue gas emissions were summed up over pilot, startup, standby, and shutdown operations for this typical day.

Wall Furnace Tested		Average Energy Use and Emission Rates				
				со	NOx	тнс
Model	Field Sites	Btu/Day	kWh/Day	lbm/MMBtu	lbm/MMBtu	lbm/MMBtu
1753012 (condensing direct vent)	Hayward 3 & 4	13853	0.070	0.021	0.086	0.001
AC2030TN #1 (single-sided low NOx)	LA 104-107	24206	0.009	0.028	0.015	0.170
AC2030TN #2 (single-sided low NOx)	LA 104-107	22246	0.011	0.127	0.012	0.010
AC3040TN (double-sided low NOx)	Oakland SFH	29204	0.009	0.270	0. <mark>039</mark>	0.018
TG2030TN (self-powered low NOx)	Sacto 4, 19	21987	0.000	0.031	0.013	0.006
	Average	22299	0.020	0.096	0.033	0.041

Table 12: Energy Use and Emission Rates for a Typical Day of Operation

Not surprisingly, the largest capacity Williams AC3040TN furnace is estimated to use the most natural gas, and the smallest capacity Williams 1753012 furnace would use the least natural gas. The 1753012 furnace also uses the most electricity.

The Williams AC3040TN furnace had the highest CO emission rate due to relatively high CO emissions during steady state operation.

The Williams 1753012 condensing furnace had the highest NOx emissions of these retrofit furnaces, due to high NOx emissions during steady state heating operation. The other three retrofit models were all low NOx furnaces, and substantial effort from the manufacturer appears to have gone into reducing their NOx emissions, as seen when comparing to the 1753012 condensing furnace emissions.

The AC2030TN #1 furnace had a high total hydrocarbon emission rate, while the AC2030TN #2 furnace had low hydrocarbon emissions. The #1 furnace appears to have had a small natural gas leak which may be representative of leaks in actual installations.

There are no standards or regulations for emissions from wall furnaces. However, as detailed in Appendix A, the South Coast Air Quality Management District and the San Joaquin Valley Air Pollution Control District require central furnaces to keep nitrogen oxide emissions below 0.033 Ibm/MMBtu. The AC2030TN and TG2030TN furnaces stay below this limit, while the AC3040TN furnace just exceeds the NOx limit. The 1753012 condensing furnace has an NOx emission rate that is 2.5 times the limit.

### **Summary and Next Steps**

Tests of retrofit wall furnaces found the following:

- Average input capacity is 109% of rated capacity, with all furnaces using more natural gas than their rating indicated
- On average, the retrofit furnaces draw about 25 W of power, but there was a lot of variation in the electricity use from furnace to furnace, and during active heating and standby operations
- These tests yielded thermal efficiency and AFUE lower than rated values for all the retrofit furnaces. On average thermal efficiency was about 4% below rated efficiency and average AFUE was about 3% below rated AFUE.
- In the non-condensing retrofit furnaces, nitrogen oxide emissions were below or just slightly over the central furnace limit of 0.033 lbm/MMBtu designated by two California air quality districts.

Overall emissions from these retrofit furnace remain quite complicated to predict, as they are not just dependent upon how much natural gas is burned. Emissions also depend on how often furnaces start up and shut down, and whether their operating cycles last long enough to reach steady state conditions.

In next steps associated with the project, the laboratory results documented in this study are used together with analysis of field monitoring results to perform additional estimates of energy use and emissions for retrofit wall furnaces. Comparisons will also be made with baseline wall furnace laboratory testing and field monitoring to estimate energy savings, emissions reductions, and indoor air quality improvements of more efficient wall furnaces.

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- Baseline Wall Furnace Laboratory Test Report Improving the Performance of Wall Furnaces in California
- Retrofit Wall Furnace Laboratory Test Report Improving the Performance of Wall Furnaces in California
- Baseline Wall Furnace Field Monitoring Report Improving the Performance of Wall Furnaces in California
- Retrofit Wall Furnace Field Monitoring Report Improving the Performance of Wall Furnaces in California
- Wall Furnace Technology Transfer Report Improving the Performance of Wall Furnaces in California
- Final Wall Furnace Report Improving the Performance of Wall Furnaces in California

## Appendix A: Related Efficiency, Emissions, and Indoor Air Quality Information

## **Wall Furnace Characteristics**

A wall furnace is a compact device used to heat a small number of rooms. Because they are less expensive, simpler to install, and take up less space than a central ducted furnace, they are commonly used in multifamily apartment complexes and smaller single-family homes. Wall furnaces are typically installed within the stud cavity of an interior wall. They exhaust combustion gases through a flue stack running vertically up to a roof penetration. They use continuously operating pilot lights to fire the main burner when calls for heating are made, and usually do not even need an electrical connection.

Wall furnaces are categorized by how they distribute heat, where their combustion air comes from, how they ignite the burner, and whether they use condensing technology. Heated air from wall furnaces can be distributed in two different ways. **Gravity** furnaces heat the air around the furnace, causing it to rise and distribute itself throughout a space naturally. This gravity-induced air flow can be supplemented by adding a booster fan, with the fan separately connected to AC power. **Fan-type** wall furnaces integrate a fan directly into the wall furnace unit to distribute heated air. The energy used by these fans can vary from 0.8 to 5 amps of single-phase AC current at 120 V depending on the capacity of the wall furnace and the efficiency of the fan.

Wall furnace combustion air is also be handled in different ways. A **vented** or **top vent furnace** draws combustion air from inside the house, then exhausts combustion gases directly to the outside. This furnace is located between the studs of an interior wall, and exhaust gases are sent through a flue of six or eight inches in diameter that travels vertically through the wall cavity to the roof. In contrast, **direct vent** furnaces draw combustion air from outside. They're generally placed in an outside wall to keep their intake ducts short, although they can be installed in an inside wall by using the proper duct extensions. Exhaust gases can also be sent outside horizontally through the wall or vertically through the wall cavity to the roof.

Three different technologies exist to ignite wall furnaces. The oldest and least efficient ignition technology is a **standing pilot**. This device uses a small burner that stays lit continually, ready to ignite the main burner whenever there is a call for heating. The standing pilot stays on by heating a thermopile which sends current to keep the pilot gas valve open. If the pilot goes out the thermopile cools off and stops sending current, and the pilot gas will stop flowing. An **intermittent pilot**, developed after the oil crisis of the 1970s, is lit only when a call for heating is made. The intermittent pilot uses an electronic spark to first light a pilot flame and then the pilot flame lights the main burner. Use of an intermittent pilot is said to reduce furnace energy use by about 5% on average. A **hot surface igniter** also uses electricity to light the furnace, but it lights the burner directly by heating a silicon nitride ceramic probe to 2000-2500°F. While heating up, the hot surface igniter draws 2 to 4 amps of current at 120 V.

While standard furnaces vent hot combustion gases outside, **condensing** furnaces run combustion air through a heat exchanger to heat incoming air. This cools the exhaust to temperatures under 100°F so that its water vapor condenses into a liquid. Condensing furnaces must be connected to drains so the condensate water is removed from the building. Additionally, furnaces can be either **single-sided** to serve just one room, or **double-sided** to serve rooms on either side of the wall in which it is installed.

## **Wall Furnace Efficiency Standards**

From 1982 through 1995, wall furnaces were regulated under ANSI Z21.49 for Gas-Fired Gravity and Fan Type Vented Wall Furnaces [ANSI Z21.49 1995]. In 1996, ANSI Z21.49 was made inactive and ANSI Z21.86 for Vented Gas-Fired Space Heating Appliances [ANSI Z21.86 2016] became the regulating standard for wall furnaces. This standard was most recently updated in 2016.

Both the Z21.49 and Z21.86 standards mandated that wall furnace nameplates list their input and output capacity based on standard test methods. The latest Z21.86 standard mandates for thermal efficiency (output capacity divided by input capacity) are listed in Table 13. The date when these minimum thermal efficiency standards were first introduced was unable to be confirmed, but they were probably part of the ANZI Z21.49-1986 update.

# Table 13: Minimum Wall Furnace Thermal Efficiency Requirement from ANSI Z21.86-2016

	<b>Gravity Wall Furnaces</b>	Fan-Type Wall Furnaces
Minimum Thermal Efficiency	70%	75%

In addition, minimum Annual Fuel Utilization Efficiency (AFUE) levels for wall furnaces are mandated under the Code of Federal Regulations for furnaces manufactured after 1990 [CFR 430.32 2022. (i) (1)] and furnaces manufactured after 2013 [CFR 430.32 2022. (i) (2)]. Table 14 lists the current minimum AFUE requirements for new wall furnaces. AFUE minimums were raised by at least 2% for furnaces manufactured after 2013.

Furnace Type	Input Capacity	AFUE 1990	AFUE 2013
Gas Wall Gravity	up to 10,000 Btu/hr	59%	
Gas Wall Gravity	over 10,000 up to 12,000 Btu/hr	60%	-
Gas Wall Gravity	over 12,000 up to 15,000 Btu/hr	61%	65%
Gas Wall Gravity	over 15,000 up to 19,000 Btu/hr	62%	
Gas Wall Gravity	over 19,000 up to 27,000 Btu/hr	63%	
Gas Wall Gravity	over 27,000 up to 46,000 Btu/hr	64%	66%
Gas Wall Gravity	over 46,000 Btu/hr	65%	67%
Gas Wall Fan-Type	up to 42,000 Btu/hr	73%	75%
Gas Wall Fan-Type	over 42,000 Btu/hr	74%	76%

# Table 14: Minimum AFUE Requirements for Wall Furnacesmanufactured after January 1, 1990 and April 16, 2013

Thermal efficiency and AFUE are both measures of a furnace's efficiency, but they represent different furnace operations. Thermal efficiency represents the full-load performance of a system, while AFUE represents the performance over a typical range of operating conditions. Many of the baseline furnaces in this study were manufactured before AFUE ratings were required. While all rated and tested AFUE values are reported, furnace efficiency comparisons rely mostly on thermal efficiency values.

Wall furnaces are located inside the building envelope, and all top vent furnaces use indoor air for combustion. This means that their performance tends to stay relatively constant under different weather conditions as compared to furnaces that sit in unconditioned or semiconditioned spaces. It also means that laboratory-measured efficiencies should be fairly good job of predicting actual efficiency of wall furnaces as they operate in the field.

## **Related Emissions and Indoor Air Quality Guidelines**

Like all gas burning equipment, even properly operating wall furnaces produce low levels of CO, NOx and particulate matter emissions. As with all primary gas space heating equipment in the state of California, emissions are required to be vented to the outside to prevent the accumulation of indoor pollutants.

There are no federal or California limits on flue gas emissions or indoor pollutants generated by wall furnaces. However, the Code of Federal Regulations limits particulate matter emissions from wood-burning residential forced-air furnaces. Residential forced-air furnaces are defined for this standard as fuel burning devices designed to burn wood or wood pellet fuel that warms a space other than the space where the furnace is located. Wall furnaces don't meet this definition because they burn natural gas, and because heat the space where they are installed.

For reference, forced-air furnaces manufactured after May 16, 2015 were required to emit no more than 0.93 lbm/MMBtu of particulate matter [CFR 2022, 60.5474 (b) (4)], defined as the total of PM2.5 and PM10 particles. This limit was lowered to 0.15 lbm/MMBtu in total particulate matter for forced-air furnaces manufactured after May 15, 2020 [CFR 2022, 60.5474 (b) (6)].

In California, the South Coast Air Quality Management District (SCAQMD) and the San Joaquin Valley Air Pollution Control District (SJVAPCD) limit NOx emissions from natural gas-fired fantype central furnaces distributed or sold in their territories. These standards do not specifically define a central furnace. It is typically a furnace that heats air in one place and circulates it through ducts to other places, so these rules do not apply to wall furnaces. For reference, both the SCAQMD Rule 1111 [SCAQMD 2021] and SJVAPCD Rule 4905 [SJVAPCD 2020] require furnaces to keep NOx emissions, on a basis of NO2, below 14 ng/Joule (0.033 lbm/MMBtu).

The US Environmental Protection Agency does not regulate indoor air quality, but they have characterized typical levels of carbon monoxide found in homes (US EPA CO 2022). They have not agreed upon standards for nitrogen oxides (US EPA NOx 2022) or particulate matter (US EPA PM 2022) within homes but have laid out acceptable levels for these pollutants in outside air over different time periods.

The US Environmental Protection Agency has developed guidelines for outdoor air quality, the National Ambient Air Quality Standards (US EPA NAAQS 2022), with acceptable limits of outdoor air pollutants in terms of averages over different time periods. The California Air Resources Board has also developed standards for outdoor air quality that are sometimes more stringent than federal standards, the California Ambient Air Quality Standards (CARB CO 2022, CARB NOX 2022, CARB PM 2022).

Table 15 summarizes the regulations, standards, and guidelines for residential furnaces and indoor air quality, as well as some outdoor air pollution standards. Although none of these standards applies to wall furnaces, they serve as reference values for this project's emissions and indoor air quality analyses. Note that no regulations, standards, or guidelines were identified that help characterize hydrocarbon emissions.

Rule	Equipment	CO	NOx	PM2.5 & PM10
Code of Federal Regulation	Residential forced-air furnaces, wood-burning	n/a	n/a	0.93 lbm/MMBtu, 2015 0.15 lbm/MMBtu, 2020
SCAQMD Rule 1111 & SJVAPCD Rule 4905	Central furnaces	n/a	0.033 lbm/MMBtu (14 nanograms/Joule)	n/a
US EPA reference levels of typical indoor air pollutants	Indoor air quality in homes	0 - 5 ppm normal 5 - 15 ppm near properly adjusted gas stove 30 ppm or more near improperly adjusted gas stoves	n/a	n/a
National Ambient Air Quality Standards	Outside air	9 ppm 8 hours 35 ppm 1 hour	100 ppb 1 hour 53 ppb 24 hours	PM2.5 35 ug/m <sup>3</sup> 24 hours PM10 150 ug/m <sup>3</sup> 24 hours
California Ambient Air Quality Standards	Outside air	9 ppm 8 hours 20 ppm 1 hour	180 ppb I hour 30 ppb 24 hours	PM2.5 none 24 hours PM10 50 ug/m3 24 hours

#### Table 15: Emissions and Indoor Air Quality Regulations, Standards and Guidelines

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