



## **INTERIM PROJECT REPORT**

## Baseline Wall Furnace Laboratory Test Report -Improving the Performance of Wall Furnaces in California

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This is an interim report for CEC-PIR-18-005, "Improving the Performance of Wall Furnaces in California", a project designed to yield gas savings by replacing existing wall furnaces with more efficient retrofit models. This project gathers information about furnace performance, operation, emissions, and indoor air quality from laboratory testing and field monitoring of baseline and retrofit wall furnaces.

### Background

It is estimated that there are 1.4 million wall furnaces in California. Wall furnaces were introduced in California as early as 1930 and gained prevalence in single-family homes and low-rise multifamily residential buildings as primary or auxiliary sources of heating. Not infrequently wall furnaces are as old as the buildings they occupy and may not have safety switches to prevent the furnaces from overheating. The oldest existing furnaces have rated thermal efficiencies of 50% while most standard replacement wall furnaces have rated thermal efficiencies of 70%.

More advanced wall furnaces achieve rated thermal efficiencies of 80% to 94% by eliminating pilot lights, using more efficient heat exchangers, and incorporating condensing or modulating technology. This means there is a substantial savings potential for a state-wide replacement program that promotes furnaces using these efficiency advancements.

This interim report documents test results for baseline wall furnaces that were removed from California homes for laboratory testing. Other interim reports for this project document field monitoring of these existing baseline furnaces, laboratory test results for more efficient retrofit furnaces, and field monitoring of retrofit furnaces that replaced the baseline furnaces.

### **Project Purpose and Approach**

The goal of this research is to demonstrate cost-effective solutions for retrofitting existing wall furnaces in California multifamily and single-family residences. This interim report gives the results of baseline wall furnace laboratory testing to characterize the energy use, efficiency, and flue gas emissions of a sample of baseline wall furnaces. Other reports document results of retrofit wall furnace laboratory testing, and field monitoring results of baseline and retrofit wall furnaces.

The baseline wall furnaces studied in this project were existing furnaces that had been in service in California homes. The furnaces were initially monitored in the field over a heating season, then were removed and shipped to Des Plaines, IL facilities for testing in GTI Energy's Residential and Commercial Equipment laboratory.

Ten baseline vented gravity wall furnaces were tested:

- Two from side-by-side apartments in Hayward (apartments 3 and 4)
- Four from a retirement apartment community in Los Angeles (apartments 104, 105, 106, and 107)
- One from a single-family home in Oakland (SFH)

• Three from multifamily apartments in Sacramento (apartments 4, 15, and 19)

These ten existing wall furnaces were all vented gravity non-condensing furnaces with standing pilots. These furnaces ranged in age from about 10 years to more than 40 years with rated input capacities between 25,000 and 50,000 Btu/hr and rated thermal efficiencies from 50% to 74%. The Oakland furnace was a double-sided unit serving two rooms, while all other furnaces were single-sided units. After field monitoring each of these furnaces over a winter heating season, they were removed from service and shipped to GTI Energy's Des Plaines facility for laboratory testing.

Laboratory testing included measurement of furnace natural gas flow, electricity use, operating temperatures, and concentrations of carbon monoxide (CO), nitrogen oxides (NOx), and total hydrocarbons (THC) in exhaust gases. The testing protocol covered furnace operation during standby, startup, steady state, and shutdown. Parameters derived from measurements include each furnace's input capacity and pilot gas use, efficiency, and pollutant emission rates.

### **Key Results**

Table 1 lists the rated and measured natural gas flows of each wall furnace. All but one of the furnaces used less natural gas than their rated input, for an average 89% of rated input. Gas use of the standing pilot was either ~500/750/1000 Btu/hr and tended to be greater for furnaces with larger input capacity.

	Wall Furnace Tested				Natural Gas Input			
Manufacturer	Model	Field Site	Age years	Rated Btu/hr	Tested Btu/hr	% Rated Input	Pilot Btu/hr	
Perfection Products	PW8G25SEN #1	Hayward 3 Baseline	~40	25000	20280	81%	<mark>5</mark> 20	
Perfection Products	PW8G25SEN #2	Hayward 4 Baseline	~40	25000	20210	81%	5 <mark>1</mark> 0	
Williams	25GV-A1	LA 104 Baseline	~35	25000	25100	100%	750	
Williams	35GV-C #1	LA 105 Baseline	~35	35000	31720	91%	<mark>5</mark> 20	
Williams	35GV-C #2	LA 106 Baseline	~35	35000	31800	91%	<mark>57</mark> 0	
Williams	RMG35-IN	LA 107 Baseline	~35	35000	31810	91%	5 <mark>00</mark>	
Williams	5009622	Oakland SF Baseline	~15	50000	44500	89%	1090	
Holly General	35S-D #1	Sacramento 4 Baseline	40+	35000	31530	90%	720	
Holly General	35S-D #2	Sacramento 15 Baseline	40+	35000	29110	83%	710	
Williams 3509622 Sacramento		Sacramento 19 Baseline	~10	35000	33800	97%	1050	
		Average		33500	30000	89%	<mark>69</mark> 0	

Table 1: Baseline Wall Furnace Natural Gas Input Rates

Table 2 lists the rated and test-derived thermal efficiency and AFUE for each unit. Rated AFUE values are only listed for the two furnaces manufactured after the minimum AFUE reporting requirement was put into place January 1, 1990. Six of the tested furnaces exceeded their thermal efficiency ratings while four did not. Six furnaces also exceeded the 70% minimum thermal efficiency required by the American National Standards Institute regulations (ANSI Z21.86 2016), and five met the 65% minimum AFUE required by the Code of Federal Regulations (CFR 430.32 2022).

Таріс	Table 2. Dasenne Wan Furnace mermai Enciency and AFOL							
Wa		Thermal Efficiency		AF	UE			
Manufacturer	Model	Field Site	Rated	Tested	Rated	Tested		
Perfection Products	PW8G25SEN #1	Hayward 3	70%	76.3%		70.5%		
Perfection Products	PW8G25SEN #2	Hayward 4	70%	71.8%		66.1%		
Williams	25GV-A1	LA 104	70%	70.5%		64.4%		
Williams	35GV-C #1	LA 105	70%	62.8%		<b>59.2</b> %		
Williams	35GV-C #2	LA 106	70%	73.6%		69.3%		
Williams	RMG35-IN	LA 107	70%	75.1%		71.1%		
Williams	5009622	Oakland SFH	76%	<b>50.</b> 1%	74.0%	<b>46.</b> 0%		
Holly General	35S-D #1	Sacramento 4	<b>50</b> %	<b>39.0%</b>		<b>35.7%</b>		
Holly General	35S-D #2	Sacramento 15	<b>50</b> %	60.8 <mark>%</mark>		<b>56.2</b> %		
Williams	3509622	Sacramento 19	74%	73.2%	72.0%	66.7%		
		Average	67.0%	<b>65.3%</b>		60.5 <mark>%</mark>		

Table 2: Baseline Wall Furnace Thermal Efficiency and AFUE

Table 3 lists the energy use and emissions for each wall furnace for a typical day of operation as found during field testing of these units, where the furnace cycles 1.5 times a day for 33 minutes per cycle and remains in standby with the pilot light on for the rest of the day. As expected, the largest capacity unit in this study, the 50,000 Btu/hr Oakland unit, would use the most natural gas. The 35,000 Btu/hr Sacramento 19 furnace used a lot of natural gas relative to its capacity due to its high pilot gas use while in standby.

	for a Typical Day of Operation								
Wal	Wall Furnace Tested				Average Energy Use & Emission Rates at Each Site				
Manufacturer	Model	Field Site	Btu/Day	CO Btu/Day lbm/MMBtu		THC lbm/MMBtu			
Perfection Products	PW8G25SEN #1	Hayward 3	28 <mark>782</mark>	0.194	0.081	0.054			
Perfection Products	PW8G25SEN #2	Hayward 4	28 <mark>493</mark>	0.037	0.072	0.327			
Williams	25GV-A1	LA 104	38089	0.116	0.063	0.255			
Williams	35GV-C #1	LA 105	38220	0.086	0.075	0.006			
Williams	35GV-C #2	LA 106	39445	0.039	0.059	0.000			
Williams	RMG35-IN	LA 107	37831	0.061	0.071	0. <mark>147</mark>			
Williams	5009622	Oakland SF	61973	0.333	0.077	0.006			
Holly General	35S-D #1	Sacramento 4	42698	0.067	0.069	0.005			
Holly General	35S-D #2	Sacramento 15	40470	0.596	0.019	0.029			
Williams	Villiams 3509622 Sacramento 19		52219	0.059	0.090	0. <mark>143</mark>			
		Average	40822	0.169	0.068	0.087			

Table 3: Baseline Wall Furnace Energy Use and Emission Ratesfor a Typical Day of Operation

There are no regulations for gravity wall furnace emissions, but two California air quality districts limit central furnace nitrogen oxides (NOx) emissions to 0.033 lbm/MMBtu, the South Coast Air Quality Management District's Rule 1111 (SCAQMD 2021) and the San Joaquin Valley

Air Pollution Control District's Rule 4905 (SJVAPCD 2020). Only one of the baseline wall furnaces would comply with this limit, the Holly General 35S-D unit from Sacramento 15, one of the two oldest furnaces tested in this project. On average, NOx emissions from these baseline wall furnaces were twice the regulated limit for central furnaces. NOx emissions from these furnaces were generated during active heating operation due to poor control of the fuel-air ratio.

Carbon monoxide and hydrocarbon emissions are not regulated for wall furnaces or central furnaces. Laboratory testing showed variation in these emissions between furnaces, with high CO emissions from three of the tested furnaces, and high hydrocarbon emissions from four furnaces. High CO and THC emissions are usually due to incomplete combustion during startup and shutdown, although the Holly General 35S-D #2 furnace produced high CO and THC emissions while actively heating.

### **Knowledge Transfer and Next Steps**

The laboratory results documented in this study will be combined with results from the field monitoring of these baseline furnaces to determine energy use and emissions from typical baseline wall furnaces. Similar laboratory testing and field monitoring will be done to characterize the performance of more efficient retrofit furnaces. Baseline and retrofit data will then be used to estimate the energy savings and emission reduction potential of more efficient wall furnaces.

## Introduction

This project's overall objective is to characterize the operation, energy, indoor air quality, and emissions of existing and retrofit wall furnaces. The goal of this research is to investigate and demonstrate efficient solutions for retrofitting existing wall furnaces in California multifamily and single-family residences.

A wall furnace is a compact device installed within a home's wall cavity and used to heat one or two rooms. Because they are less expensive, simpler to install, and take up less space than a central ducted furnace, they are used in multifamily apartment complexes and smaller single-family homes.

Wall furnaces are categorized by how they distribute heat (gravity or fan-type), where their combustion air comes from (from inside for top vent furnaces, from outside for direct vent furnaces), how they ignite the burner (standing pilot, intermittent pilot, or hot surface igniter), and whether they use condensing technology. Additionally, furnaces can be either single-sided to serve just one room, or double-sided to serve rooms on either side of the wall in which it is installed. These wall furnace technologies are described in more depth in Appendix A.

Many California low-rise multifamily buildings and smaller homes use wall furnaces for space heating. Most of these existing wall furnaces are non-condensing gravity vented furnaces that use a standing pilot to ignite the burner. Wall furnaces are usually replaced only when the original unit is irreparably broken. Anecdotal information from Williams, the predominant wall furnace manufacturer, indicates that many older furnaces are still in operation, some without safety switches and with rated thermal efficiencies as low as 50%.

Most replacement wall furnaces are non-condensing gravity vented furnaces that just meet current efficiency standards. ANSI Z21.86 for Vented Gas-Fired Space Heating Appliances (ANSI Z21.96 2016) is the federal regulating standard for wall furnaces, It currently requires gravity wall furnace thermal efficiency to be at least 70% and fan-type wall furnace efficiency to be at least 75%. In addition, Annual Fuel Utilization Efficiency (AFUE) for wall furnaces are mandated under the Code of Federal Regulations (CFR 430.32 (i) (1) 2022) and (CFR 430.32 (i) (2) 2022). AFUE must be at least 65% to 76%, depending on furnace capacity and whether it is a gravity or fan-type wall furnace. More information about wall furnace efficiency standards is included in Appendix A.

Minimum wall furnace AFUE levels are well below the 81% AFUE requirement for standard central ducted furnaces and even further below the >90% AFUE that condensing furnaces can deliver. However, wall furnaces have recently been developed with thermal efficiencies as high as 85% and AFUE up to 82%, achieved by improving burners and removing standing pilot lights. In addition, condensing wall furnaces with thermal efficiency up to 94% and AFUE as high as 93% have been developed.

As with all primary gas space heating equipment in the state of California, emissions from wall furnace combustion are required to be vented to the outside to prevent the accumulation of indoor pollutants. There are no federal or California limits for wall furnaces regarding flue gas

emissions or indoor pollutants, although there are some limits on NOx emissions for natural gas-fired fan-type central furnaces in California's South Coast Air Quality Management District (SCAQMD) and the San Joaquin Valley Air Pollution Control District (SJVAPCD). See Appendix A for information about guidelines, standards, and regulations that pertain to indoor air quality and furnace emissions.

This project examines existing baseline and efficient retrofit wall furnaces in the laboratory and the field to assess their performance, ease of installation, operation, and reliability. Energy use, emissions, indoor air quality, and costs are assessed to help determine whether efficient retrofit wall furnace technologies should be promoted in California.

This interim report describes results from laboratory tests of ten baseline wall furnaces that were removed from homes and shipped to GTI's Des Plaines facility.

- Two from side-by-side apartments in Hayward (apartments 3 and 4)
- Four from a retirement apartment community in Los Angeles (apartments 104, 105, 106, and 107)
- One from a single-family home in Oakland (SFH)
- Three from multifamily apartments in Sacramento (apartments 4, 15, and 19)

Laboratory testing involved running the furnaces through a protocol that included standby, startup, steady state, and shutdown operation while measuring:

- Inlet, outlet, and exhaust temperatures of the wall furnaces
- Carbon monoxide, nitrogen oxide, and total hydrocarbon flue gas emissions
- Natural gas flow rates

In other project work, these test results will be applied to field monitoring data for these furnaces to estimate their energy use and emissions. Efficient retrofit furnaces will also be laboratory tested and field monitored as part of this project. Comparisons of baseline and retrofit energy use and emissions will be made to evaluate the savings that can be realized through the installation of more efficient retrofit furnaces.

Laboratory testing was conducted within the Residential and Commercial Equipment laboratory on the Des Plaines, IL GTI Energy campus. Wall furnace tests included measurement of intake, burner and exhaust temperatures, natural gas and electricity use, and exhaust gas emission levels.

### **Furnaces Tested**

This project tested a total of ten baseline wall furnaces which had been in active use at various California sites. These furnaces were shipped to GTI Energy for laboratory testing after they were removed and replaced with more efficient retrofit furnaces. The characteristics of each baseline furnace are presented in Table 4.

Field Site	Manufacturer	Model*	ANSI Z21 Std	Age years	Input Btu/hr	Thermal Efficiency	Rated AFUE
Hayward 3	Perfection Products	PW825SEN-B-4 #1	49a.1982	~40	25,000	50%	n/a
Hayward 4	Perfection Products	PW825SEN-B-4 #2	49a.1982	~40	25,000	50%	n/a
Los Angeles 104	Williams	25GV-A1	49.1986	~35	25,000	70%	n/a
Los Angeles 105	Williams	35GV-C #1	49.1986	~35	35,000	70%	n/a
Los Angeles 106	Williams	35GV-C #2	49.1986	~35	35,000	70%	n/a
Los Angeles 107	Williams	RMG35IN	49.1986	~35	35,000	70%	n/a
Oakland SFH	Williams	liams 5009622 (Double-sided)		~15	50,000	76%	74%
Sacramento 4	ento Holly Narrowall General 35S-D #1		none	40+	35,000	70%	n/a
Sacramento 15	Holly General	Narrowall 35S-D #2	none	40+	35,000	70%	n/a
Sacramento 19			86.2008	~10	35,000	74%	72%

# Table 4: Laboratory Tested Baseline Wall Furnace Characteristics,Gravity Vented Non-Condensing Units with Standing Pilots

\* All models are single-sided except for the double-sided Williams model 5009622.

Input capacities range from 25,000 to 50,000 Btu/hr and thermal efficiencies, defined as the output capacity divided by the input capacity, are between 50% and 76%. AFUE ratings were only available for the two youngest furnaces, since they were not required to be determined for the older furnaces. The 50,000 Btu/hr furnace is a double-sided furnace that was installed

in the wall between the living and dining rooms of the Oakland single-family home. All other furnaces are single-sided.

The exact age of these furnaces could not be determined. An ANSI.Z21 standard and year is listed on most of the furnace nameplates, indicating that they range in age from about 10 to 40 years. The Holly-General furnaces installed in two Sacramento apartments have no ANSI standard included on their nameplate at all, so it is assumed they are more than 40 years old.

All the tested baseline furnaces were self-powered and used continuously fired standing pilots to light the main burner when heating was needed.

Figure 1, Figure 2, and Figure 3 show the existing baseline wall furnaces as they were installed in each California home.



Figure 1: Existing Baseline Wall Furnaces in Hayward 3 (left), Hayward 4 (middle), and Oakland SFH (right)

Figure 2: Existing Baseline Wall Furnaces in Los Angeles Apartments 104, 105, 106, and 107 (from left to right)



Figure 3: Existing Baseline Wall Furnaces in Sacramento Apartments 4 (left), \_\_\_\_\_\_15 (middle), and 19 (right)



### **Measurements and Test Equipment**

The following table details the measurement equipment used in the laboratory.

Measurement	Description	Range, Accuracy
Flow-Field Temperatures	1/8" J-type exposed bead thermocouple	32-1328°F/0-750°C, ±2.2°C
Ambient Temperature	1/8" J-type exposed bead thermocouple	32-1328°F/0-750°C, ±2.2°C

#### **Table 5: Laboratory Test Equipment**

Ambient Humidity	Omega OM-HL-SH-EX	0-100%RH, ±5%RH
Data Acquisition Modules	National Instruments Compact DAQ	-
Stack O <sub>2</sub>	Horiba PG350	Span 25% O <sub>2</sub> , ±1%
Stack CO <sub>2</sub>	Horiba PG350	Span 25% CO <sub>2</sub> , ±1%
Stack NO <sub>x</sub>	Horiba PG350	Span 100 ppm, ±1%
Stack CO	Horiba PG350	Span 500 ppm, ±1%
Stack THC	Rosemount Analytical 400A	Span 1000 ppm, 0.5ppm
Gas Flow Rate	American Meter AC250	8 pulses/ft <sup>3</sup>

While the furnaces were not installed into a wall assembly designed to mimic a typical internal wall cavity, GTI Energy's Des Plaines laboratory technicians followed all other ANSI Z21.86 test protocols for measurement of temperatures, exhaust gas emissions, and natural gas flow.

Inlet temperatures were measured using a thermocouple in the center of the furnace inlet grill at the bottom of each furnace.

Exhaust air temperatures were measured approximately three inches from the combustion air outlet using a probe inserted into the exhaust air duct, with three thermocouples to measure temperatures across the duct span.

Burner outlet temperature measurements were recorded using an array of nine equally spaced thermocouples, following the dimensions outlined in section 11.6.1 of ANSI Z21.86 (ANSI Z21.86 2016) to ensure an average reading in the case of a heterogeneous flow field. The burner thermocouple array was attached to the center of the burner outlet to measure temperatures of the heated air leaving the furnace.

A continuous measurement of exhaust constituents, including oxygen (O<sub>2</sub>), carbon dioxide (CO<sub>2</sub>) carbon monoxide (CO), nitrogen oxides (NO<sub>X</sub>), and unburned total hydrocarbons (THC) were measured and reported on a dry basis. Emission measurements were made through a system of three 0.25-inch stainless steel inserts in a manifold arrangement in the stack downstream of the flue temperature and pressure measurements. The emission sample points were arranged to account for exhaust streams that are non-homogenous. Combustion products were drawn through a vacuum pump and passed through a series of desiccants to provide a dry sample to a bank of analyzers located within the laboratory. Each analyzer was calibrated before each test run against a "zero" gas of pure nitrogen and then against a span gas measured in an independent analyzer.

GTI's laboratory measures the composition of the natural gas used for testing every two weeks. Samples of the natural gas being used for combustion are analyzed through a calorimeter. Although variations in gas characteristics tend to be small, the latest available house gas data was used for analysis of each tested wall furnace.

Natural gas for all wall furnace tests was delivered at a pressure of 6.9 inches water column, at the high end of the recommended 5 to 7 inches water column range for each furnace.

### **Test Procedure**

The following operating procedure was followed for wall furnace tests:

- Start up all test measurement equipment
- Calibrate all sensors following equipment manufacturer procedures
- Adjust gas supply pressure to 6.8 inches water column
- Begin recording measurements
- Light furnace pilot
- Leave furnace on standby with the pilot lit for 30 minutes to record any pilot and/or electrical energy use
- Cold start start up furnace and allow it to run for 45 minutes (steady state operation from cold start is usually reached in less than 30 minutes)
- Turn off furnace and let it sit in standby with the pilot lit for 1.5 minutes
- Hot start start up furnace again and let it run for 30 minutes (steady state operation from a hot start is usually reached in less than 20 minutes)
- Turn off furnace and leave on standby with pilot lit for 15 minutes
- End test

This entire procedure took about two hours and allowed for the measurement of the furnace in standby, startup, steady state, and shutdown operating modes. For retrofit furnaces without pilot lights, standby operating times at the beginning and end of the test were reduced since this time was not needed to measure pilot light natural gas use.

### **Data Corrections**

The gas analyzer and burner data acquisition system are separate pieces of equipment operating on slightly different time stamps. In addition, the flow of exhaust gases to the analyzer added a time delay. Data from the gas analyzer was synchronized with burner temperatures by lining up changes in  $O_2$  and  $CO_2$  concentrations with exhaust temperature changes over time.

The following corrections were made to the collected data:

- O<sub>2</sub> concentration maximum was adjusted to 20.9%, down from as much as 21.3% within +/- 1% measurement accuracy
- CO<sub>2</sub> concentration was adjusted to match the corrected O2 concentration during combustion based on the house natural gas characteristics
- CO and NOx minimum concentrations were adjusted to 0.0% (up from -0.13 ppm which is within +/- 1% measurement accuracy)

CO, NOx, and THC concentrations are reported as absolute values, and not corrected to a standard  $O_2$ % concentration as is sometimes done with furnace and boiler emissions.

 $O_2$ % varied from 10% to 19% for the baseline furnaces due to their no longer being welltuned. To report actual emissions from these furnaces in their existing condition, emission concentrations were not standardized.

### Analysis of Test Data

The fuel input capacity of the pilot light and during active combustion is operating was calculated from the measured gas flow rate as follows:

Qin = Fuel input capacity  $Btu/hr = 60 \times Active Gas$  Flow Rate x Heating Value/Timestep

Qp= Pilot Btu/hr = 60 x Standby Gas Flow Rate x Heating Value / Timestep

Active Gas Flow Rate,  $ft^3$  = measured value during active combustion

Standby Gas Flow Rate,  $ft^3$  = measured during standby conditions

Heating value,  $Btu/ft^3$  = from house natural gas used during testing

Timestep = time between measurements in minutes

Emission mass flow rates are normalized to the gas input rate from their absolute measured concentrations as follows:

Equation 1. Converting Emission Concentration to Emission Rate Emission Rate,  $Ibm/MMBtu = Concentration \times Molecular Weight \times Fd \times 20.9$ (20.9 - O<sub>2</sub>%) × Molar Volume

Concentration, ppm = absolute measured pollutant concentration

Molecular weight, lbm/lbmole = 28.0097 for CO, 46.0047 for NOx as NO2, and 16.04206 for Total Hydrocarbons (THC) as methane

Fd, lbm/MMBtu =  $10^{6} \times (3.64 \times \%H + 1.53 \times \%C + 0.57 \times \%S + 0.14 \times \%N - 0.46 \times \%O)$ /HHV, using dry weight percentages of each element in the house natural gas used for testing

 $O_2\%$  = adjusted oxygen percentage in exhaust stream

HHV, Btu/lbm = higher heating value of house natural gas used for testing

Molar Volume, dry ft<sup>3</sup>/lbmole = 385.3 at 68°F and 1 atmosphere

Estimated test thermal efficiency and AFUE are calculated for steady state operation based on Title 10 of the Code of Federal Regulations, Appendix O, Subpart B, Part 430 (CFR 430.32 2022), using the following equations:

Test  $\eta_{SS-WT}$  automatic = 100 - Ls ss - L la

Test  $\eta_{SS-WT}$  manual =  $\eta_{SS-WT}$  – L i on

Overall Test  $\eta_{SS-WT} = (\eta_{SS-WT} \text{ automatic} + \eta_{SS-WT} \text{ manual}) / 2$ 

Test AFUE automatic =  $[0.968 \text{ x} \eta_{SS-WT}] - 1.78D_f - 1.89D_s - 129P_f - 2.8L_J + 1.81$ 

Test AFUE manual = [ 2950 x  $\eta_{ss-wt}$  x  $\eta_{part \ load}$  x Qin] / [2950 x Qin + 2.083 x 4600 x  $\eta_{part}$  load x Qp

Overall Test AFUE = (Test AFUE automatic + Test AFUE manual) / 2

 $\eta_{SS-WT}$  = weighted-average steady state efficiency =  $100 - L_{L,A} - L_{s,SS}$ 

 $L_{L,A}$  = latent heat loss = 9.55 for natural gas fueled furnaces

- $L_{S,SS}$  = sensible heat loss at steady state =  $C(R_{T,S} + D)(T_{S,SS} T_{RA})$ where C = 0.0175, D = 0.171
- $R_{T,S}$  = actual to stoichiometric air mass flow rate = A + B/X<sub>co2</sub> where A = 0.0919, B = 10.96, and X<sub>co2</sub> is the concentration of carbon dioxide present in dry stack gas
- T<sub>S,SS</sub> = steady state flue gas temperature

 $T_{RA}$  = ambient room temperature

 $D_f$  = off-cycle flue gas factor = 1 for atmospheric burner type furnaces

 $D_s$  = off-cycle stack gas factor and is equal to zero for direct vent furnaces

 $P_f$  = pilot fraction =  $Q_p/Q_{in}$ 

 $L_j$  = jacket loss for floor furnaces, which is zero in this study

 $\eta_{\text{part load}}$  = part load utilization efficiency =  $\eta_{\text{SS-WT}} - L_{\text{I ON}}$ 

 $L_{i\,\text{ON}}$  = on cycle infiltration heat loss = (70-45) x (100 x Cp x S/F) x (1+ Rts x (A/F) / HHV

Cp = specific heat of air, 0.24 Btu/lbm R

S/F = stack/mass flow ratio = 1.0

A/F = stoichiometric air-fuel ratio = 14.45 for natural gas

Note that the test apparatus was not installed in a fabricated wall assembly as designated in ANSI Z21.86 2016, therefore this report's efficiencies are not official rating tests and are for informational and comparative purposes only.

Unlike central furnaces which are most often allowed to cycle automatically to meet a thermostat setting, wall furnaces are much more likely to be turned on and off manually when occupants want heating. To reflect this operation, thermal efficiency and AFUE were found as the average of the efficiency for heaters that are automatically controlled and the efficiency for heaters with manual controls.

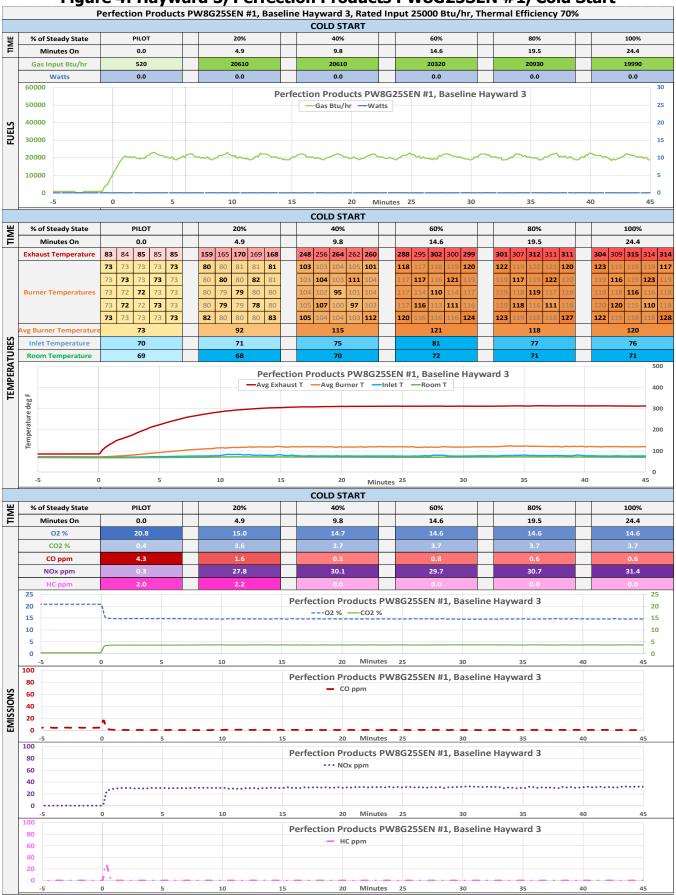
## Results

Laboratory test results are presented here for each baseline wall furnace. Data for each furnace is presented in standardized plots that show their operation during testing. Two pages of test result plots are shown for each of the ten baseline furnaces:

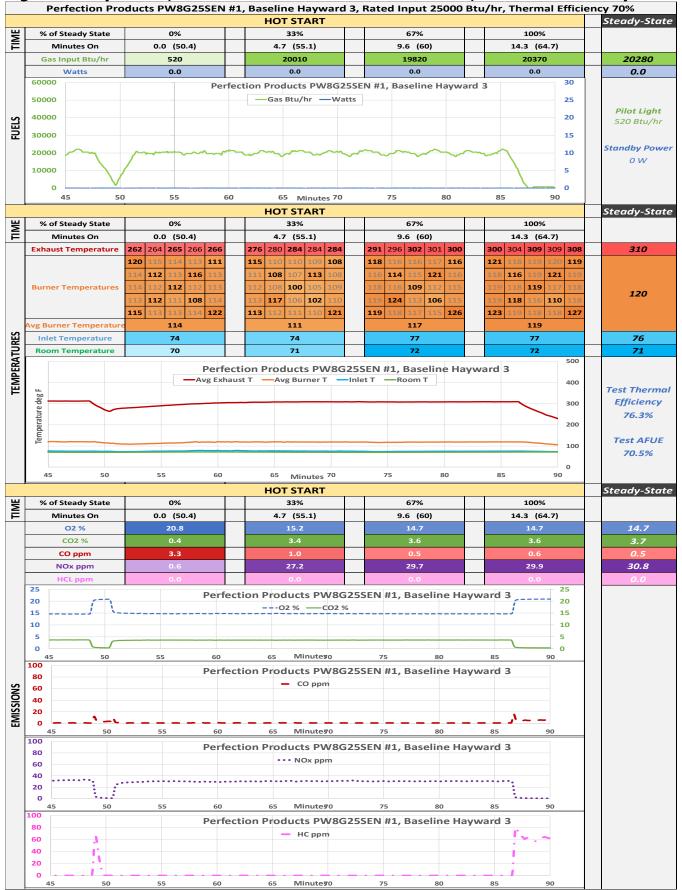
- Cold start operation including five minutes of standby operation beforehand
- Hot start operation plus a summary of steady state conditions

Each page of test results includes the following information:

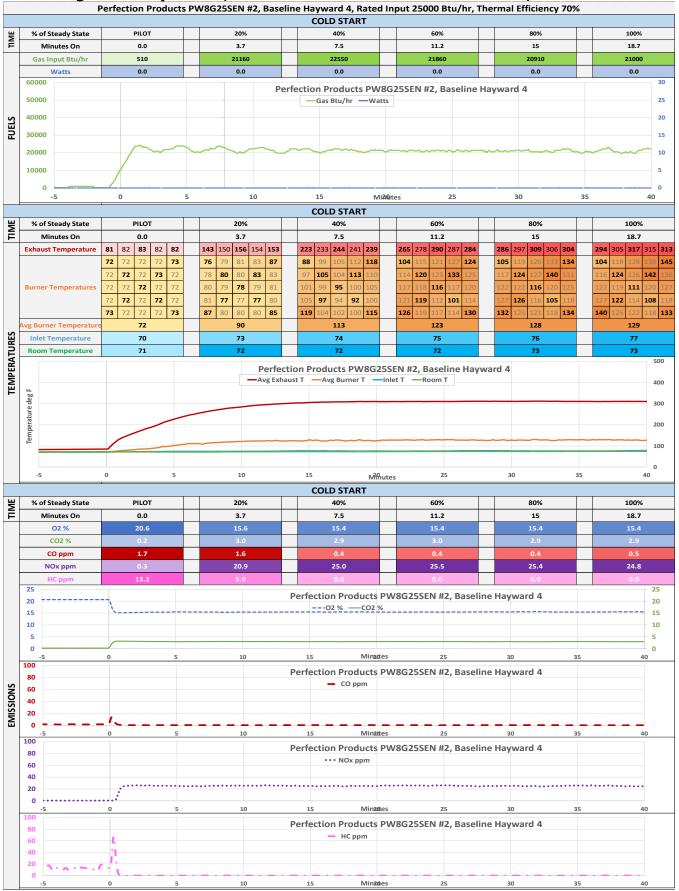
- Time to reach steady state and measured values at time intervals of 0%, 20%, 40%, 60%, 80% and 100% of steady state for the cold start, and values at time intervals of 0%, 33%, 67%, and 100% of steady state time for the hot start
- Fuel use, including both natural gas use and electrical power draw
- Exhaust, burner, inlet, and room temperatures
- Exhaust gas concentrations including O2%, CO2%, and CO, NOx, and THC concentrations in parts per million
- Note that vertical scales vary on emissions plots to show their values more clearly



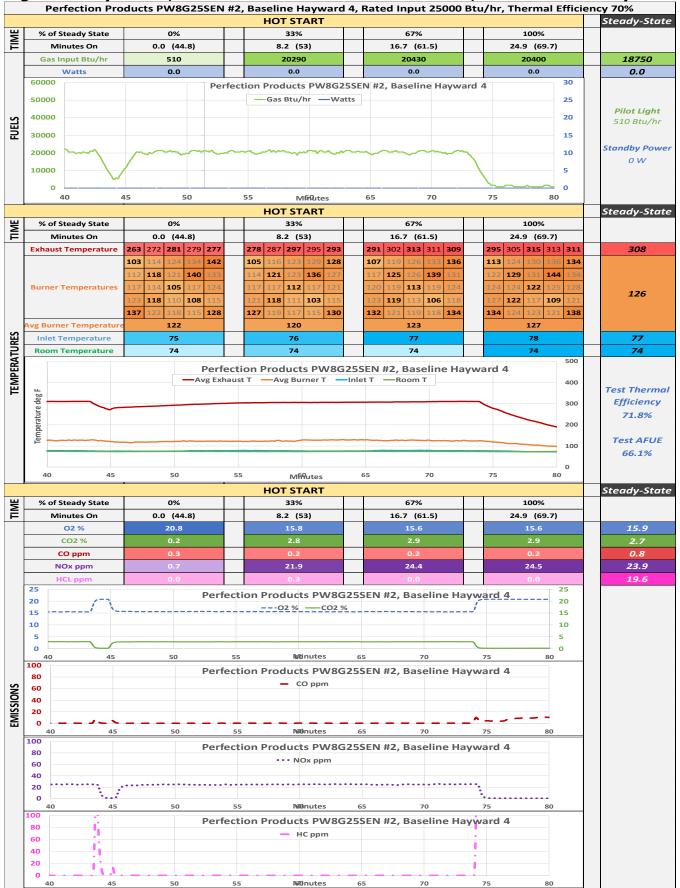
#### Figure 4: Hayward 3, Perfection Products PW8G25SEN #1, Cold Start



#### Figure 5: Hayward 3, Perfection Products PW8G25SEN #1, Hot Start & Steady state



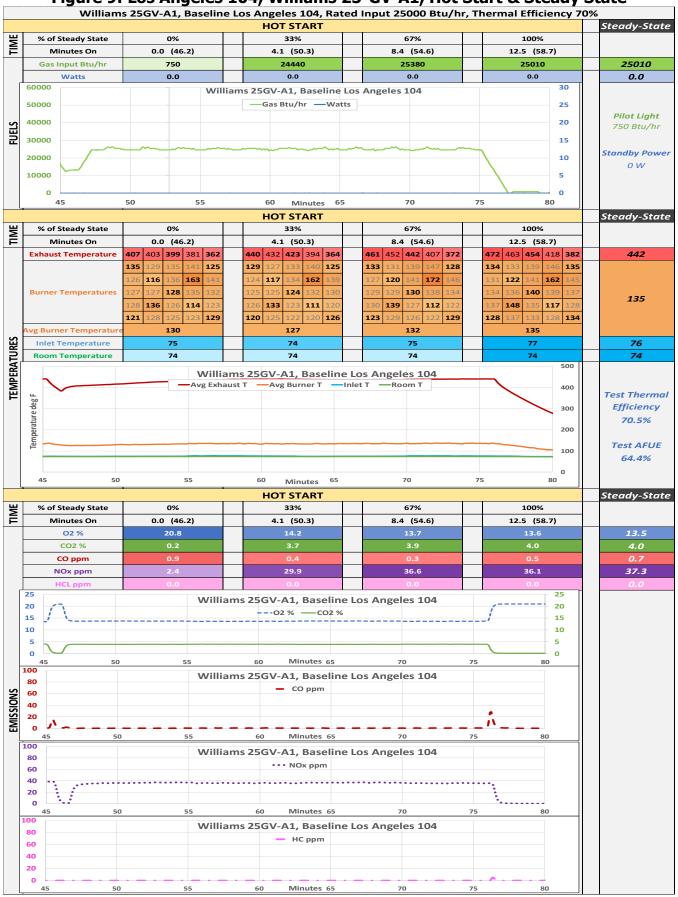
#### Figure 6: Hayward 4, Perfection Products PW8G25SEN #2, Cold Start



#### Figure 7: Hayward 4, Perfection Products PW8G25SEN #2, Hot Start & SteadyState

			LUS Angeles	COLD START			
ш	% of Steady State	PILOT	20%	40%	60%	80%	100%
TIME	Minutes On	0.0	4.7	9.4	14.1	18.8	23.5
Т				<b>418</b> 411 <b>404</b> 365 <b>325</b>	<b>465</b> 456 <b>446</b> 411 <b>376</b>		<b>478</b> 468 <b>458</b> 426 <b>39</b> 3
	Exhaust Temperature Burner Temperatures	98         98         95         93           74         74         75         75         75           74         75         75         76         75           74         74         73         74         75           74         74         73         74         75           74         74         73         74         74           75         74         74         74         74	264         261         259         227         195           81         91         100         109         94           86         89         105         129         109           88         90         97         105         102           90         84         90         89         94           95         90         92         94         103	418         411         404         565         325           113         120         132         145         121           113         111         136         178         144           116         116         118         133         129           118         120         114         104         114           119         117         116         114         123	405         446         411         376           128         128         137         147         126           124         116         140         173         146           128         129         132         138         134           131         141         127         109         122           132         130         126         122         129	475         466         456         423         390           132         134         140         149         129           127         118         142         174         148           131         132         135         141         137           134         144         131         115         126           124         133         130         126         132	4/8         4/6         4/8         4/6         4/8         4/6         39:           131         131         139         1/7         131         132         131         132         132         132         132         132         135         137         140         133           136         147         133         115         127         134         135         131         127         134
	Avg Burner Temperature	74	116	128	133	135	135
ES	Inlet Temperature	71	71	73	75	75	76
UR.	Room Temperature	72	72	72	72	73	73
TEMPERATURES	Temperature deg F			ms 25GV-A1, Baseline Lo aust T — Avg Burner T — Inl			500 400 300 200
	Tempe						100
	-5 (	) 5	10 15	5 20 Minute	<sub>25</sub> 25 30	35 40	0 45
				COLD START			
IE	% of Steady State	PILOT	20%	40%	60%	80%	100%
TIME	Minutes On	0.0	4.7	9.4	14.1	18.8	23.5
	02 % CO2 % CO ppm	20.7 0.3 3.4	13.8 4.1 1.0	13.4 4.1 0.6	13.4 4.1 1.1	13.4 4.1 1.2	13.4 4.1 1.1
	NOx ppm	0.1	28.0	39.0	40.5	40.5	39.8
	HC nnm           25           20           15           10           5           0	11 0	10	Williams 25GV-A1, Bas 02 %	eline Los Angeles 104		25 20 15 10 5 0
	-5 100	0 5	10 1		25 30	35 40	45
EMISSIONS	80 60 40 20 0			Williams 25GV-A1, Bas — CO ppm	eline Los Angeles 104		
Ξ	-5 100 80	0 5	10 1	5 20 Minutes Williams 25GV-A1, Bas ••• NOx ppm	25 30 eline Los Angeles 104	35 40	45
	60 40 20 0			••••••••••	••••		• • • • • • • • • • • • •
	-5	0 5	10 1	5 20 Minutes	25 30	35 40	45
	100           80           60           40			Williams 25GV-A1, Bas — HC ppm	eline Los Angeles 104	l	
	20						
	-5	0 5	10 1	5 20 Minutes	25 30	35 40	45

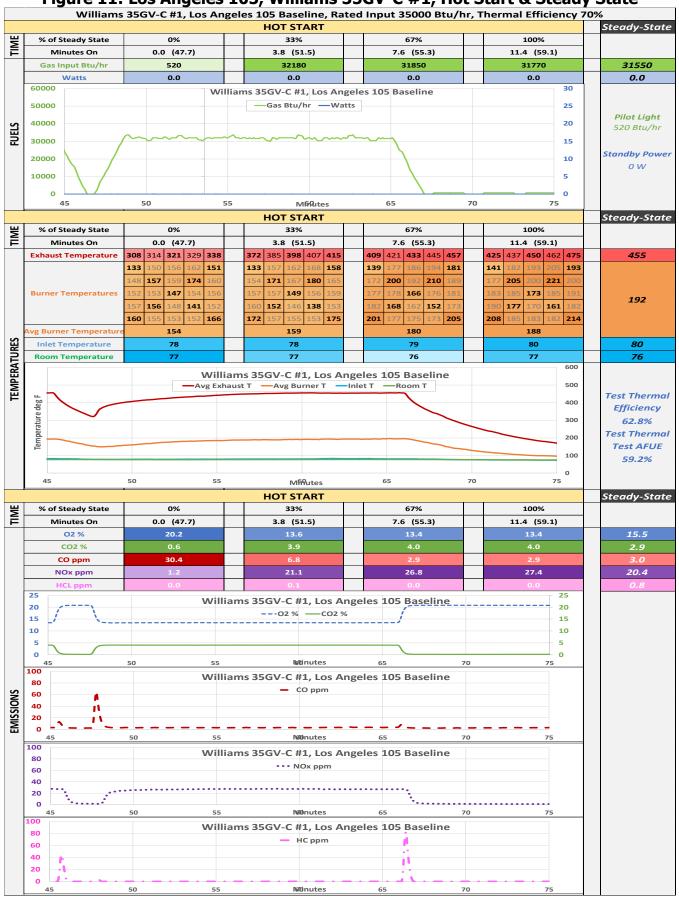
### Figure 8: Los Angeles 104, Williams 25-GV-A1, Cold Start



#### Figure 9: Los Angeles 104, Williams 25-GV-A1, Hot Start & Steady State



#### Figure 10: Los Angeles 105, Williams 35GV-C #1, Cold Start

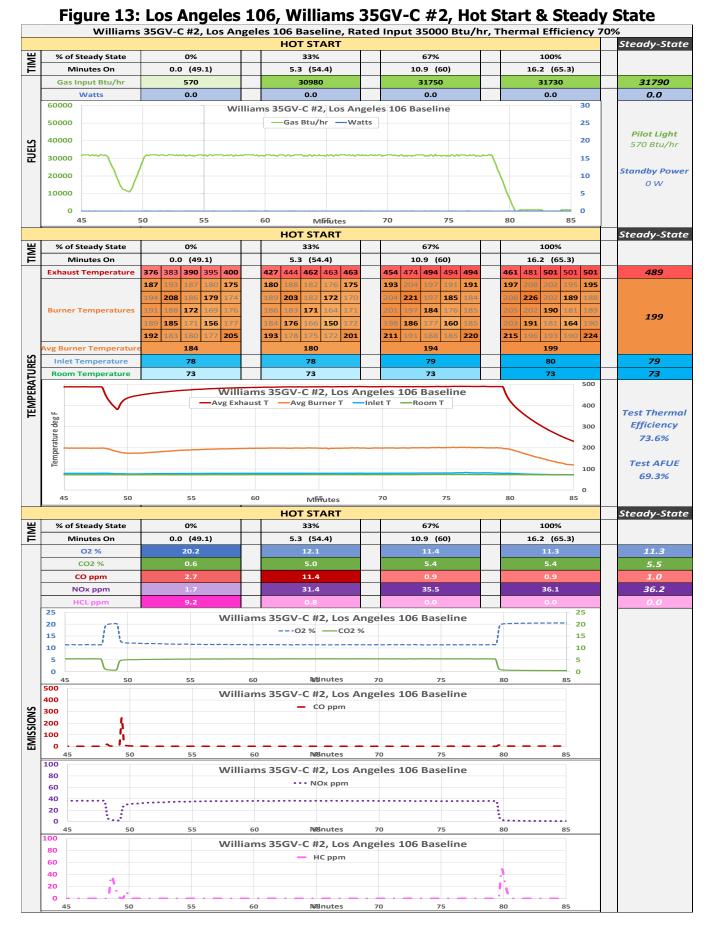


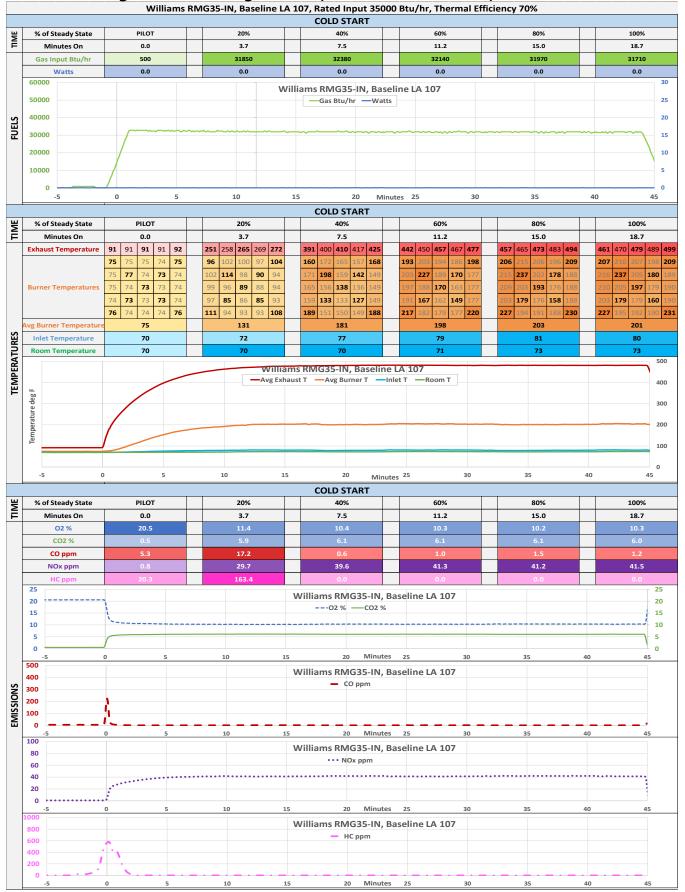
#### Figure 11: Los Angeles 105, Williams 35GV-C #1, Hot Start & Steady State

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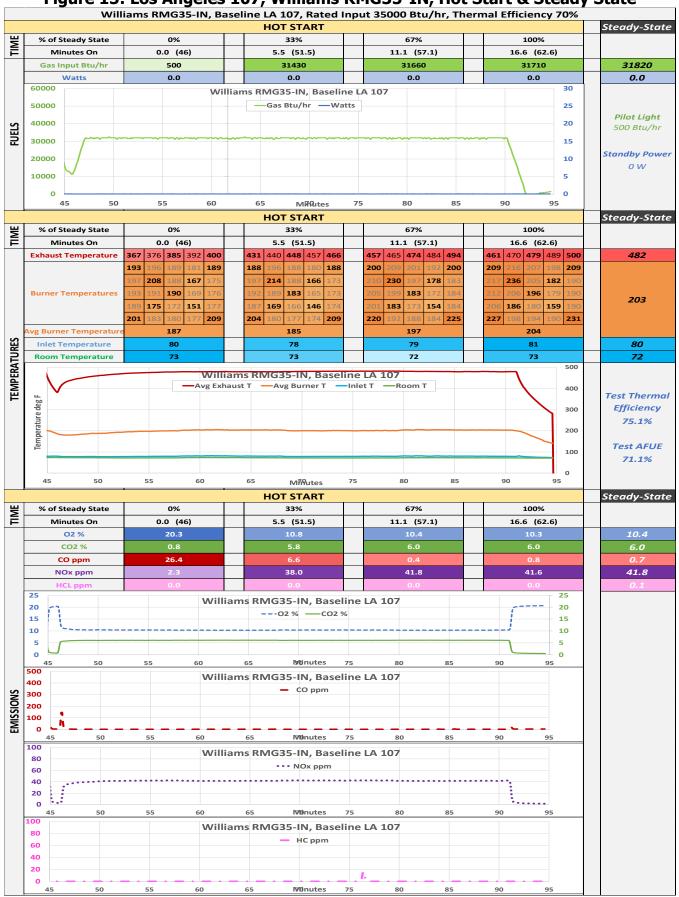


#### Figure 12: Los Angeles 106, Williams 35GV-C #2, Cold Start



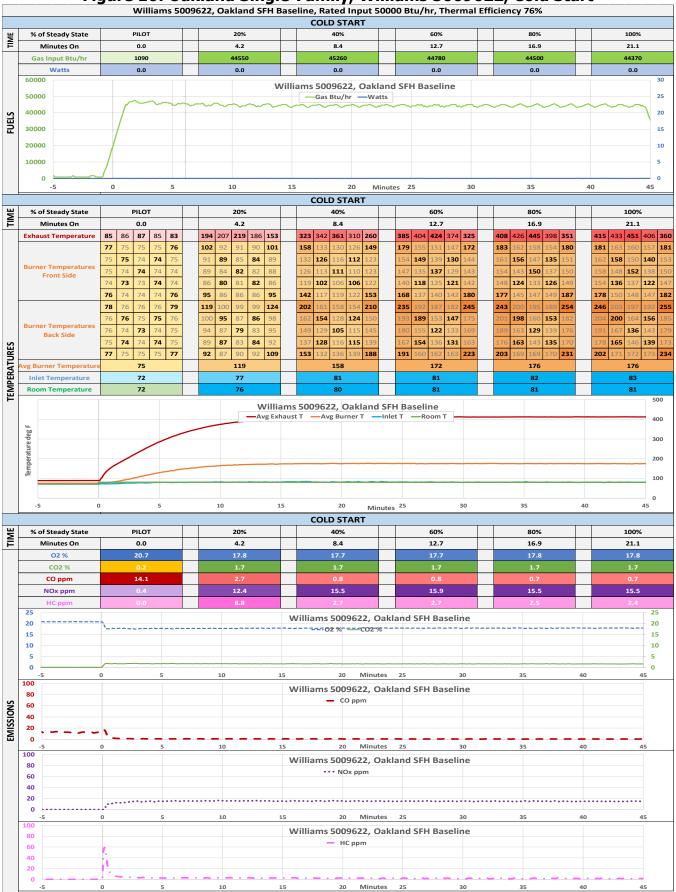


#### Figure 14: Los Angeles 107, Williams RMG35-IN, Cold Start

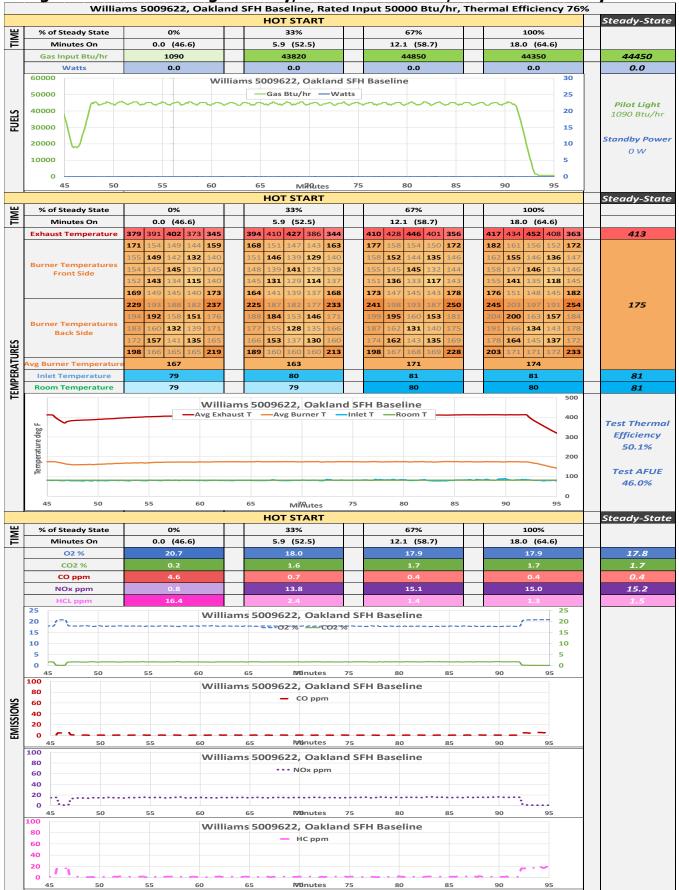


#### Figure 15: Los Angeles 107, Williams RMG35-IN, Hot Start & Steady State

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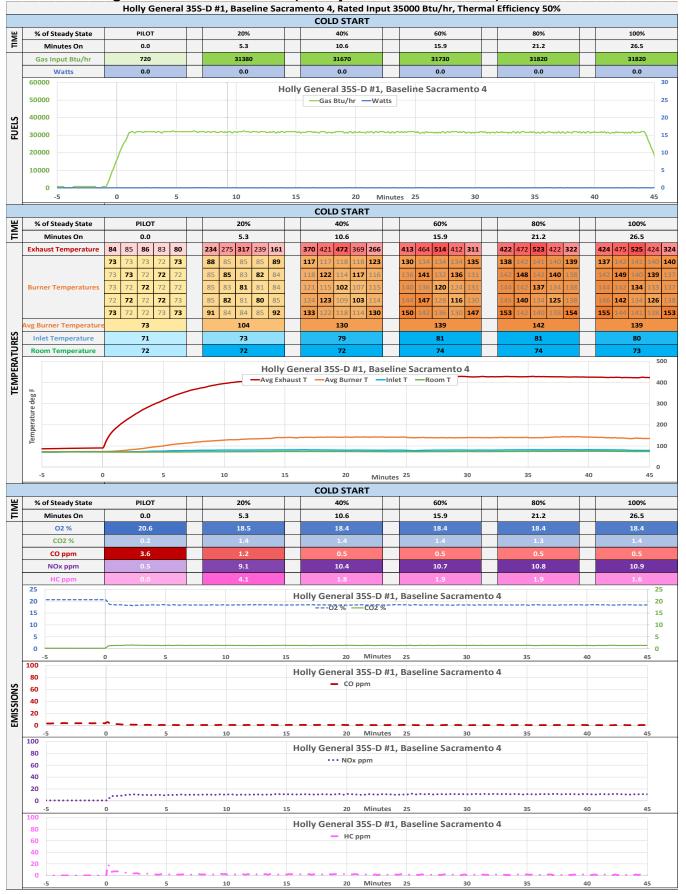


#### Figure 16: Oakland Single-Family, Williams 5009622, Cold Start

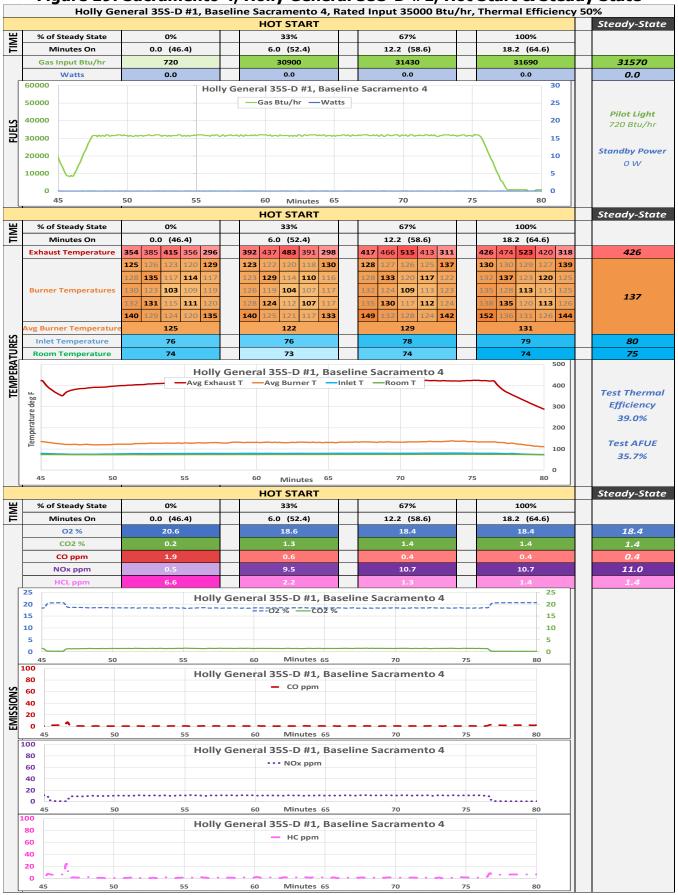


#### Figure 17: Oakland Single-Family, Williams 5009622, Hot Start & Steady State

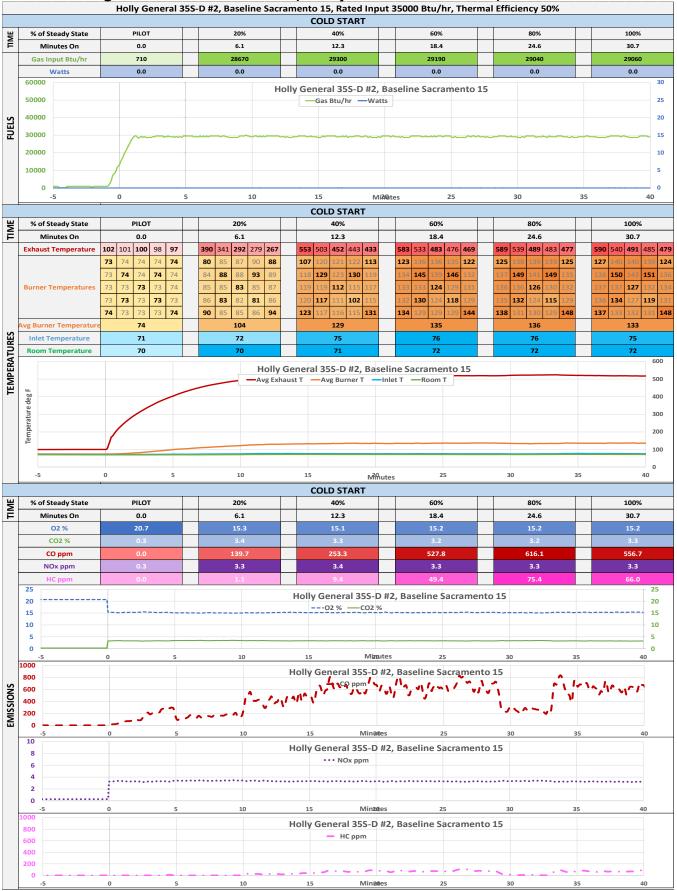
29



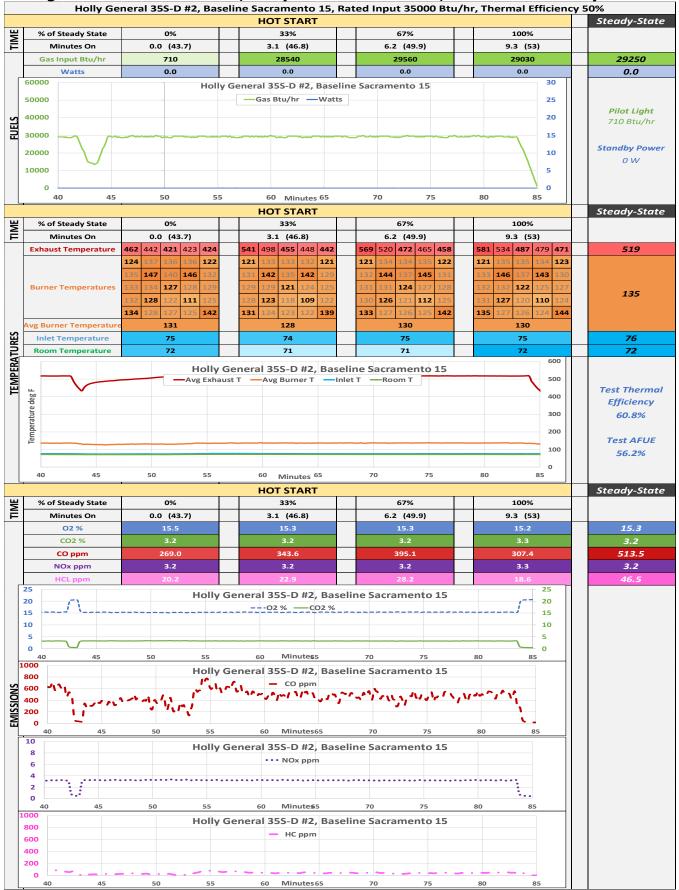
#### Figure 18: Sacramento 4, Holly General 35S-D #1, Cold Start



#### Figure 19: Sacramento 4, Holly General 35S-D #1, Hot Start & Steady State

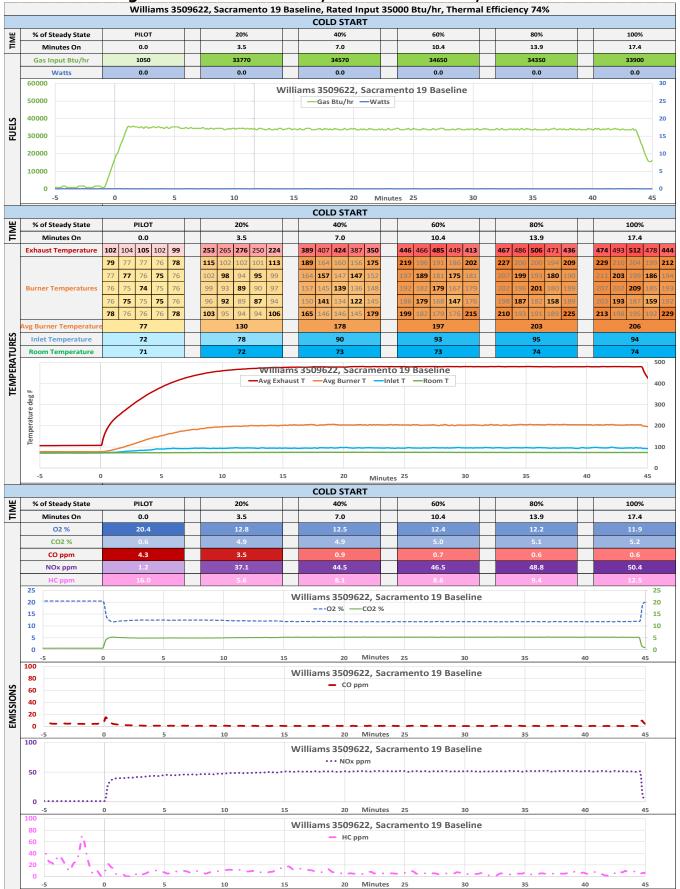


#### Figure 20: Sacramento 15, Holly General 35S-D #2, Cold Start

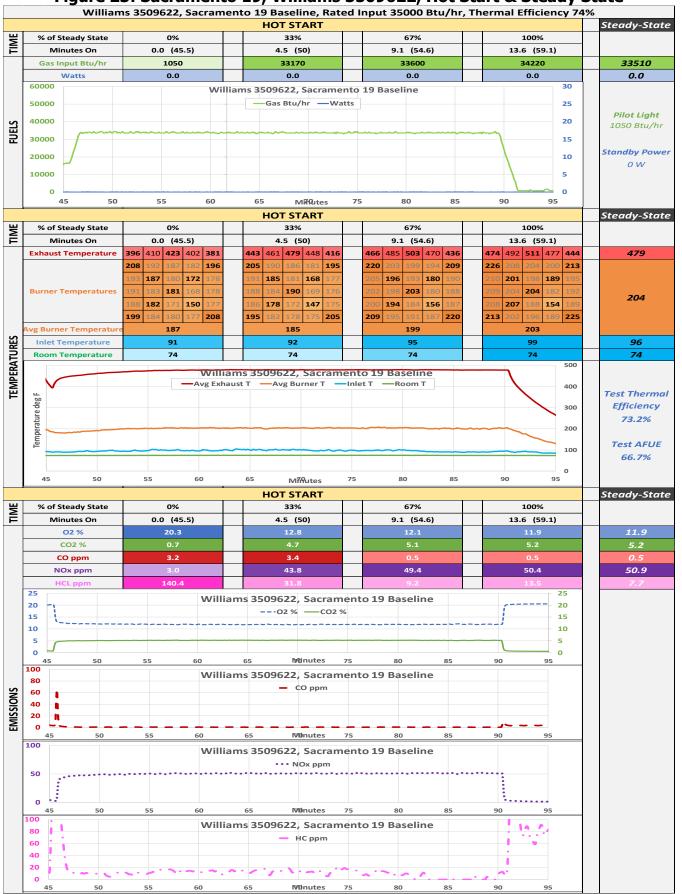


#### Figure 21: Sacramento 15, Holly General 35S-D #2, Hot Start & Steady State

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#### Figure 22: Sacramento 19, Williams 3509622, Cold Start



#### Figure 23: Sacramento 19, Williams 3509622, Hot Start & Steady State

Below laboratory test results are compared for all ten baseline wall furnaces, including their fuel use, combustion and thermal characteristics, efficiency, and emissions.

### **Baseline Wall Furnace Fuel Use**

Table 6 lists the measured fuel input for all tested wall furnaces, including both natural gas use during active firing and during pilot-only standby conditions as well as the rated input capacity. Note that a gas pressure of 6.8 inches water column was used during all testing, at the high end of the recommended 5 to 7 inches water column range for each furnace.

Wall Furnace Tested					latural Gas	Input	
Manufacturer	Model	Field Site	Age years	Rated Btu/hr	Tested Btu/hr	% Rated Input	Pilot Btu/hr
Perfection Products	PW8G25SEN #1	Hayward 3 Baseline	~40	25000	20280	81%	<mark>5</mark> 20
Perfection Products	PW8G25SEN #2	Hayward 4 Baseline	~40	25000	20210	81%	<mark>5</mark> 10
Williams	25GV-A1	LA 104 Baseline	~35	25000	25100	100%	750
Williams	35GV-C #1	LA 105 Baseline	~35	35000	31720	91%	<mark>5</mark> 20
Williams	35GV-C #2	LA 106 Baseline	~35	35000	31800	91%	<mark>57</mark> 0
Williams	RMG35-IN	LA 107 Baseline	~35	35000	31810	91%	<mark>5</mark> 00
Williams	5009622	Oakland SF Baseline	~15	50000	44500	89%	1090
Holly General	35S-D #1	Sacramento 4 Baseline	40+	35000	31530	90%	720
Holly General	35S-D #2	Sacramento 15 Baseline	40+	35000	29110	83%	710
Williams	3509622	Sacramento 19 Baseline	~10	35000	33800	97%	1050
		Average		33500	30000	89%	690

#### Table 6: Baseline Wall Furnace Natural Gas Input Rates

All baseline furnaces except the Williams 25GV-A1 furnace used less natural gas than their rated value, with the oldest furnaces using as little as 81% of their rated input. This indicates that over time the furnace gas valves were clogged or can no longer open fully, and therefore tend to restrict the amount of gas flow.

All baseline units used pilot lights to ignite the burner, drawing between 500 and 1090 Btu/hr. Pilot use seems to settle into ~500, ~700, and ~1,000 Btu/hr pilot use classifications corresponding to 25,000, 35,000 and 50,000 Btu/hr capacity furnaces. But there are three exceptions, with Williams 25GV-A1 falling into the 700 Btu/hr class, Williams RMG35-IN into the 500 Btu/hr class, and Williams 3509622 into the 1,000 Btu/hr class.

## **Baseline Wall Furnace Combustion and Thermal Characteristics**

Table 7 lists the percentages of oxygen and carbon dioxide found in the exhaust gases of each wall furnace, which is an indicator of combustion efficiency. Oxygen levels around 13.5% and carbon dioxide around 4% indicate that the fuel-air ratio is neither too rich nor too lean for good combustion. While on average the baseline furnaces have adequate combustion, four operated above 15% O2 and below 3.5% CO2, and three operated below 12.5% O2 and

above 5% CO2. This means that seven of ten furnaces were not operating with proper fuel-air ratios.

	Comb	ustion		
Manufacturer	Manufacturer Model Field Site		% 02	% CO2
Perfection Products	PW8G25SEN #1	Hayward 3 Baseline	14.8	3.6
Perfection Products	PW8G25SEN #2	Hayward 4 Baseline	15.6	2.8
Williams	25GV-A1	LA 104 Baseline	13.6	4.0
Williams	35GV-C #1	LA 105 Baseline	14.2	3.6
Williams	35GV-C #2	LA 106 Baseline	11.9	5.2
Williams	RMG35-IN	LA 107 Baseline	10.5	5.9
Williams	5009622	Oakland SF Baseline	17.8	1.7
Holly General	35S-D #1	Sacramento 4 Baseline	18.4	1.4
Holly General	35S-D #2	Sacramento 15 Baseline	15.3	3.3
Williams	3509622	Sacramento 19 Baseline	12.2	5.1
		Average	14.4	3.7

#### Table 7: Combustion Exhaust Gas Oxygen and Carbon Dioxide Percentages

Table 8 lists the time to reach steady state conditions during cold and hot starts for each tested furnace. Steady state conditions were assumed to be reached when the average exhaust temperature first rose to within 3°F of the maximum temperature achieved during each respective cold or hot start.

Wall Furnace Tested			Minutes to	Steady-State	Steady State Conditions			
Manufacturer	Model	Field Site	Cold Start	Hot Start	Exhaust °F	Burner °F	Inlet °F	Room °F
Perfection Products	PW8G25SEN #1	Hayward 3 Baseline	24.4	14.3	<u>310</u> .3	<b>11</b> 9.5	76.0	70.7
Perfection Products	PW8G25SEN #2	Hayward 4 Baseline	18.7	24.9	308.3	125.7	77.1	73.8
Williams	25GV-A1	LA 104 Baseline	23.5	12.5	441.9	135.3	76.1	73.6
Williams	35GV-C #1	LA 105 Baseline	24.2	11.4	454.9	192.3	80.4	76.4
Williams	35GV-C #2	LA 106 Baseline	1 <mark>6.7</mark>	1 <mark>6.2</mark>	488.8	198.9	79.3	72.8
Williams	RMG35-IN	LA 107 Baseline	18.7	1 <mark>6.6</mark>	481.7	202.7	80.0	72.4
Williams	5009622	Oakland SF Baseline	21.1	18.0	412.5	175.3	81.4	80.9
Holly General	35S-D #1	Sacramento 4 Baseline	26.5	18.2	425.7	137.2	80.4	74.6
Holly General	35S-D #2	Sacramento 15 Baseline	30.7	9.3	519.2	135.3	75.9	72.4
Williams	3509622	Sacramento 19 Baseline	17.4	13.6	479.0	204.1	95.9	74.0
		Average	22.2	15.5	432.2	<b>162.</b> 6	80.3	74.2

#### Table 8: Baseline Wall Furnace Steady State Conditions, deg F

Steady state was reached within 16 to 31 minutes during cold starts, and within 9 to 25 minutes during hot starts. In all but one furnace, the cold start took longer to reach steady state than the hot start. The exception is Perfection Products PW8G25SEN #2, where it took about six more minutes to reach steady state during the hot start than during the cold start.

Table 8 also lists the average cold start and hot start steady state exhaust, burner, inlet, and room temperatures reached for each furnace. Room temperatures varied since the test facility was not isolated in a climate-controlled room. Inlet temperatures to each furnace tended to be higher than the room temperature, indicating that the furnaces entrain some of the heat they

produce directly back into the unit. This entrainment may have been affected by a lack of conditioning and air circulation in the test facility. Average exhaust temperatures vary by more than 200°F, from 308°F to 519°F, and burner temperatures vary from 120°F to 204°F.

## **Baseline Wall Furnace Efficiency**

Table 9 lists the rated and tested thermal efficiency and Annual Fuel Utilization Efficiency (AFUE) of each wall furnace. Note that these are not official rated values since the furnaces were not installed into a fabricated wall cavity assembly as specified by the ANSI Z21.86 2016 test standard. Values in red are below the current minimum listed in Table 14 and Table 15 of Appendix A for thermal efficiency (70% for gravity furnaces) and AFUE (65% to 67%).

Table Fi Ba						
Wall Furnace Tested			Thermal Efficiency		AFUE	
Manufacturer	Model	Field Site	Rated	Tested	Rated	Tested
Perfection Products	PW8G25SEN #1	Hayward 3	70%	76.3%		70.5%
Perfection Products	PW8G25SEN #2	Hayward 4	70%	71.8%		66.1%
Williams	25GV-A1	LA 104	70%	70.5%		64.4%
Williams	35GV-C #1	LA 105	70%	<b>62.8</b> %		<b>59.2</b> %
Williams	35GV-C #2	LA 106	70%	73.6%		69.3%
Williams	RMG35-IN	LA 107	70%	75.1%		71.1%
Williams	5009622	Oakland SFH	76%	<b>50.</b> 1%	74.0%	<b>46.</b> 0%
Holly General	35S-D #1	Sacramento 4	<b>50</b> %	<b>39.0%</b>		35.7%
Holly General	35S-D #2	Sacramento 15	<b>50</b> %	60.8 <mark>%</mark>		<b>56.2</b> %
Williams	3509622	Sacramento 19	74%	73.2%	72.0%	66.7%
		Average	67.0%	<b>65.3%</b>		60.5 <mark>%</mark>

**Table 9: Baseline Wall Furnace Tested Thermal Efficiency and AFUE** 

Findings regarding wall furnace efficiency include:

- Tested thermal efficiency was within 2% of rated thermal efficiency on three units, Perfection Products PW8G25SEN #2, Williams 25GV-A1, and Williams 3509622
- Thermal efficiency was more than 2% higher than the rated thermal efficiency on four units, Perfection Products PW8G25SEN #1, Williams 35GV-C #2, Williams RMG35-IN, and Holly General 35S-D #2
- Tested thermal efficiency was well below rated thermal efficiency on three units, Williams 35GV-C #1, Williams 5009622, and Holly General 35S-D #1
- Six of the ten baseline units meet the 70% thermal efficiency standard for wall furnaces from the ANSI Z21.86 (Table 4)

Individual furnaces in identical furnace pairs fared quite differently from each other in terms of tested efficiency, as seen when comparing the pairs of Perfection Products PW8G25SEN, Williams 35GV-C, and Holly General 35S-D models. Their performance differences are likely due to the varying history of each furnace in terms of how much it was used and how well it was maintained.

The average tested thermal efficiency of all ten units was 65.3% compared to the 67% rated average, so efficiency did not fare too badly from a collective standpoint. However, individual units performed as much as 26% lower and 6% higher than their rated thermal efficiency.

According to ANSI Z21.86-2016 as listed in Table 14 in Appendix A, the minimum thermal efficiency for these gravity furnaces should be 70% and four of these ten furnaces tested below 70%. It was not expected that the two Holly General 35S-D furnaces would meet this standard, since they were manufactured before it was in effect. The Williams 35GV-C #1 and the Williams 5009622 double-sided furnace were ~7% and ~20% short of this standard.

AFUE ratings were not available for most of the baseline furnaces since these were not required before January 1, 1990, when these units were manufactured. Calculated AFUE from test data are included for informational purposes only. These calculated AFUE values were 3% to 6% lower than tested thermal efficiencies.

As listed in Table 15 in Appendix A, the minimum AFUE from the Code of Federal Regulations is 65% for the 25,000 Btu/hr furnaces, 66% for the 35,000 Btu/hr furnaces, and 67% for the 50,000 Btu/hr furnace. AFUE minimums were not reached for the same four furnaces that did not attain minimum thermal efficiency: Holly General 35S-D #1, Holly General 35S-D #2, Williams 35GV-C #1, and Williams 5009622. AFUE for the Williams 25GV-A1 furnace, at 64.4%, was just short of the required 65%.

## **Baseline Wall Furnace Emissions**

Emission concentrations for each wall furnace were measured using a gas analyzer probe inserted in the exhaust stream. Emissions during the test procedure were then averaged over four operating conditions:

- Pilot while in standby with only the pilot light burning natural gas
- Startup from the start of combustion until the average exhaust temperature reaches steady state as defined by heating up to within 2°F of the maximum temperature achieved during that test
- Steady State after the exhaust temperature reaches steady state and before the burner shuts off
- Shutdown for 1.5 minutes after gas flow to the burner is turned off and only the pilot light burning natural gas

Exhaust stream concentrations in parts per million are converted to emission mass flow rates in lbm per MMBtu using Equation 1. Note that this conversion uses the percentage of oxygen in the exhaust flow to account for the fuel input, not the measured natural gas flow itself. There are often brief high concentrations and mass flow rates of pollutants in the exhaust stream at startup and shutdown. These spikes get ameliorated because startup emissions get folded into the entire startup time to steady state, and because shutdown emissions are assumed to occur at the much lower pilot gas rate.

Table 10, Table 11, and Table 12 on the following page list the carbon monoxide, nitrogen oxides, and total hydrocarbon emission rates found during testing of each wall furnace.

As was seen in the plots of emission concentrations over time during each wall furnace test, carbon monoxide and total hydrocarbon emissions tend to be higher during startup and especially shutdown, when combustion is not complete. Nitrogen oxide emissions tend to be higher while heating is actively operating due to poor fuel-air ratios.

Wall Sumaas Tested						
Wall Furnace Tested		Carbon Monoxide, lbm/MMBtu				
Manufacturer	Model	Field Site	Standby	Startup	Steady State	Shutdown
Perfection Prod	PW8G25SEN #1	Hayward 3 Baseline	0.459	0.005	0.001	0.314
Perfection Prod	PW8G25SEN #2	Hayward 4 Baseline	0.078	0.002	0.019	0.178
Williams	25GV-A1	LA 104 Baseline	0.253	0.002	0.001	0.271
Williams	35GV-C #1	LA 105 Baseline	0.190	0.018	0.063	0.175
Williams	35GV-C #2	LA 106 Baseline	0.105	0.010	0.001	0.057
Williams	RMG35-IN	LA 107 Baseline	0.183	0.012	0.001	0.059
Williams	5009622	Oakland SF Baseline	0.809	0.008	0.002	0.261
Holly General	35S-D #1	Sacramento 4 Baseline	0.166	0.004	0.002	0.072
Holly General	35S-D #2	Sacramento 15 Baseline	0.000	0.880	1.194	1.065
Williams	3509622	Sacramento 19 Baseline	0.122	0.006	0.001	0.064
		Average	0.237	0.095	0.128	0.251

#### **Table 10: Baseline Wall Furnace Carbon Monoxide Emissions**

Table 11: Baseline Wall Furnace Nitrogen Oxides Emissions

Wall Furnace Tested			Nitrogen Oxides, lbm/MMBtu			
Manufacturer	Model	Field Site	Standby	Startup	Steady State	Shutdown
Perfection Prod	PW8G25SEN #1	Hayward 3 Baseline	0.049	0.102	0.105	0.125
Perfection Prod	PW8G25SEN #2	Hayward 4 Baseline	0.021	0.095	0.133	0.309
Williams	25GV-A1	LA 104 Baseline	0.009	0.105	0.108	0.890
Williams	35GV-C #1	LA 105 Baseline	0.038	0.073	0.113	0.414
Williams	35GV-C #2	LA 106 Baseline	0.032	0.076	0.071	0.061
Williams	RMG35-IN	LA 107 Baseline	0.045	0.081	0.084	0.091
Williams	5009622	Oakland SF Baseline	0.037	0.103	0.106	0.077
Holly General	35S-D #1	Sacramento 4 Baseline	0.036	0.088	0.093	0.045
Holly General	35S-D #2	Sacramento 15 Baseline	0.028	0.012	0.012	0.031
Williams	3509622	Sacramento 19 Baseline	0.058	0.115	0.121	0.107
		Average	0.035	0.085	0.095	0.215

#### Table 12: Baseline Wall Furnaces Total Hydrocarbon Emissions

Wall Furnace Tested		Total Hydrocarbons, Ibm/MMBtu				
Manufacturer	Model	Field Site	Standby	Startup	Steady State	Shutdown
Perfection Prod	PW8G25SEN #1	Hayward 3 Baseline	0.126	0.001	0.000	1.889
Perfection Prod	PW8G25SEN #2	Hayward 4 Baseline	0.383	0.002	0.642	6.767
Williams	25GV-A1	LA 104 Baseline	0.558	0.001	0.000	0.003
Williams	35GV-C #1	LA 105 Baseline	0.012	0.001	0.009	0.097
Williams	35GV-C #2	LA 106 Baseline	0.000	0.000	0.000	0.140
Williams	RMG35-IN	LA 107 Baseline	0.448	0.025	0.000	0.000
Williams	5009622	Oakland SF Baseline	0.000	0.014	0.004	0.586
Holly General	35S-D #1	Sacramento 4 Baseline	0.000	0.009	0.004	0.161
Holly General	35S-D #2	Sacramento 15 Baseline	0.000	0.047	0.075	0.140
Williams	3509622	Sacramento 19 Baseline	0.287	0.023	0.007	0.939
		Average	0.181	0.012	0.074	1.072

There are some clear outlying furnaces with higher emission rates:

- Holly General 35S-D #2 had high CO emissions throughout its entire test
- Williams 5009622 had large CO emissions during standby pilot-only operation
- Williams 25GV-A1 had high NOx emissions at shutdown
- Perfection Products PW8G25SEN #2's high HC emissions indicate a gas leak
- Perfection Products PW8G25SEN #1, an older model, and Williams 3509622, a newer model, also had high HC emissions

As was seen with comparisons of tested efficiencies, emissions from individual furnaces in identical furnace pairs (Perfection Products PW8G25SEN, Williams 35GV-C, and Holly General 35S-D models) were quite different from each other. Performance differences are likely due to the varying history of each furnace in terms of hours of use and maintenance.

There are no standards for emissions from wall furnaces. However, as detailed in Appendix A, the South Coast Air Quality Management District and the San Joaquin Valley Air Pollution Control District require central furnaces nitrogen oxide emissions below 0.033 lbm/MMBtu.

From Table 11, only the Holly General 35S-D #2 furnace kept below the 0.033 lbm/MMBtu NOx limit during pilot, startup, steady state, and shutdown operations. This is surprising since it is one of the oldest and least efficient furnaces in this study, and it also had high CO emissions. All the other furnaces exceed the 0.033 lbm/MMBtu NOx limit in all or most of their operating modes.

## Wall Furnace Energy Use and Emissions during Typical Operation

To investigate energy use and emissions further, Table 13 lists fuel use and emission rates over a typical day of operation for each baseline furnace. Field testing showed that the average baseline furnace was operated for 1.5 on-off cycles every day for 33 minutes per cycle. Natural gas use and flue gas emissions were summed up during pilot, startup, standby, and shutdown operations for this typical day.

Wall Furnace Tested			Average Energy Use & Emission Rates at Each Site				
Manufacturer	Model	Field Site	Btu/Day	CO lbm/MMBtu	NOx Ibm/MMBtu	THC lbm/MMBtu	
Perfection Products	PW8G25SEN #1	Hayward 3	28782	0.194	0.081	0.054	
Perfection Products	PW8G25SEN #2	Hayward 4	28493	0.037	0.072	0.327	
Williams	25GV-A1	LA 104	38089	0.116	0.063	0.255	
Williams	35GV-C #1	LA 105	38220	0.086	0.075	0.006	
Williams	35GV-C #2	LA 106	39445	0.039	0.059	0.000	
Williams	RMG35-IN	LA 107	37831	0.061	0.071	0. <mark>147</mark>	
Williams	5009622	Oakland SF	61973	0.333	0.077	0.006	
Holly General	35S-D #1	Sacramento 4	42698	0.067	0.069	0.005	
Holly General	35S-D #2	Sacramento 15	40470	0.596	0.019	0.029	
Williams	3509622	Sacramento 19	52219	0.059	0.090	0. <mark>143</mark>	
		Average	40822	0.169	0.068	0.087	

#### Table 13: Energy Use and Emission Rates for a Typical Day of Operation

Not surprisingly, the largest capacity Williams 5009622 furnace would use the most natural gas and have the highest NOx emissions. But the furnace using the least amount of natural gas, Perfection Products PW8GSEN25 #2, had the most hydrocarbon emissions. The furnace with the lowest NOx and THC emissions, Holly General 35S-D #2, had the highest CO emissions.

Only the Holly General 35S-D #2 meets the 0.033 lbm/MMBtu limit for NOx emissions. All other furnaces emit about twice the limit. It is important to remember that this limit only applies to central furnaces, not wall furnaces, but it is a useful guideline to consider when evaluating wall furnace environmental sustainability.

#### **Summary and Next Steps**

These laboratory test results show how complicated it is to estimate baseline wall furnace energy use, performance, and emissions.

Collectively, baseline furnaces input capacity is 89% of their rated capacity, average pilot gas use is 690 Btu/hr, and average thermal efficiency was about 2% below rated efficiency. However, capacity, pilot gas use, and efficiency vary from unit to unit with respect to their ratings.

Emissions are also quite complicated to predict, as they are not just dependent upon how much natural gas is burned. Emissions also depend on how often furnaces start up and shut down, and whether their operating cycles last long enough to reach steady state conditions.

In next steps associated with the project, the laboratory results documented in this study are used together with analysis of field monitoring results to perform additional estimates of energy use and emissions from this sample of baseline wall furnaces. Comparisons will be made with retrofit wall furnace laboratory testing and field monitoring to estimate energy savings, emissions reductions, and indoor air quality improvements of more efficient wall furnaces.

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- Baseline Wall Furnace Laboratory Test Report Improving the Performance of Wall Furnaces in California
- Retrofit Wall Furnace Laboratory Test Report Improving the Performance of Wall Furnaces in California
- Baseline Wall Furnace Field Monitoring Report Improving the Performance of Wall Furnaces in California
- Retrofit Wall Furnace Field Monitoring Report Improving the Performance of Wall Furnaces in California
- Wall Furnace Technology Transfer Report Improving the Performance of Wall Furnaces in California
- Final Wall Furnace Report Improving the Performance of Wall Furnaces in California

## Appendix A: Related Efficiency, Emissions, and Indoor Air Quality Information

## **Wall Furnace Characteristics**

A wall furnace is a compact device used to heat one or two rooms. Because they are less expensive, simpler to install, and take up less space than a central ducted furnace, they are used in multifamily apartment complexes and smaller single-family homes. Wall furnaces are typically installed within the stud cavity of an interior wall. They exhaust combustion gases through a flue stack running vertically up to a roof penetration. They use continuously operating pilot lights to fire the main burner when there is a call for heating, and usually do not even need an electrical connection.

Wall furnaces are categorized by how they distribute heat, where their combustion air comes from, how they ignite the burner, and whether they use condensing technology. Heated air from wall furnaces can be distributed in two ways. **Gravity** furnaces heat the air around the furnace, causing it to rise and distribute itself throughout a space naturally. This gravity-induced air flow can be supplemented by a booster fan, with the fan separately connected to AC power. **Fan-type** wall furnaces integrate a fan directly into the wall furnace unit to distribute heated air. The energy used by these fans can vary from 0.8 to 5 amps of single-phase AC current at 120 V depending on the capacity of the wall furnace and the efficiency of the fan.

Wall furnace combustion air is also handled in two ways. A **vented** or **top vent furnace** draws combustion air from inside the house, then exhausts combustion gases directly to the outside. This furnace is located between the studs of an interior wall, and exhaust gases are sent through a flue of six or eight inches in diameter that travels vertically through the wall cavity to the roof. In contrast, **direct vent** furnaces draw combustion air from outside. They are placed in an outside wall to keep their intake ducts short, although they can be installed in an inside wall by using the proper duct extensions. Exhaust gases can also be sent outside horizontally through the wall or vertically through the wall cavity to the roof.

Three different technologies exist to ignite wall furnaces. The oldest and least efficient ignition technology is a standing pilot. This device uses a small burner that stays lit continually, ready to ignite the main burner whenever there is a call for heating. The standing pilot stays on by heating a thermopile which sends current to keep the pilot gas valve open. If the pilot goes out the thermopile cools off and stops sending current, and the pilot gas will stop flowing. An intermittent **pilot**, developed after the oil crisis of the 1970s, is lit only when a call for heating is made. The intermittent pilot uses an electronic spark to first light a pilot flame and then the pilot flame lights the main burner. Use of an intermittent pilot is said to reduce furnace energy use by about 5% on average. A hot surface igniter also uses electricity to light the furnace, but it lights the burner directly by heating a silicon nitride ceramic probe to 2000-2500°F. While heating up, the hot surface igniter draws 2 to 4 amps of current at 120 V.

Thermal efficiency and AFUE are both measures of a furnace's efficiency, but they represent different furnace operations. Thermal efficiency represents the full-load performance of a system, while AFUE represents the performance over a typical range of operating conditions. Many of the baseline furnaces in this study were manufactured before AFUE ratings were required. While all rated and tested AFUE values are reported, furnace efficiency comparisons rely mostly on thermal efficiency values.

### **Wall Furnace Efficiency Standards**

From 1982 through 1995, wall furnaces were regulated under ANSI Z21.49 for Gas-Fired Gravity and Fan Type Vented Wall Furnaces (ANSI Z21.49 1995). In 1996, ANSI Z21.49 was made inactive and ANSI Z21.86 for Vented Gas-Fired Space Heating Appliances (ANSI Z21.86 2016) became the regulating standard for wall furnaces. This standard was most recently updated in 2016.

Both the Z21.49 and Z21.86 standards mandated that wall furnace nameplates list their input and output capacity based on standard test methods. The latest Z21.86 standard mandates for thermal efficiency (output capacity divided by input capacity) are listed in Table 14. The date when these minimum thermal efficiency standards were first introduced was unable to be confirmed, but they were probably part of the ANZI Z21.49-1986 update.

# Table 14: Minimum Wall Furnace Thermal Efficiency Requirement from ANSI Z21.86-2016

	Gravity Wall Furnaces	Fan-Type Wall Furnaces				
Minimum Thermal Efficiency	70%	75%				

In addition, minimum Annual Fuel Utilization Efficiency (AFUE) levels for wall furnaces are mandated under the Code of Federal Regulations for furnaces manufactured after 1990 (CFR 430.32 (i) (1) 2022) and furnaces manufactured after 2013 (CFR 430.32 (i) (2) 2022). Table 15 lists the current minimum AFUE requirements for new wall furnaces. AFUE minimums were raised by at least 2% for furnaces manufactured after 2013.

Furnace Type	Input Capacity	AFUE 1990	AFUE 2013
Gas Wall Gravity	up to 10,000 Btu/hr	59%	
Gas Wall Gravity	over 10,000 up to 12,000 Btu/hr	60%	-
Gas Wall Gravity	over 12,000 up to 15,000 Btu/hr	61%	65%
Gas Wall Gravity	over 15,000 up to 19,000 Btu/hr	62%	-
Gas Wall Gravity	over 19,000 up to 27,000 Btu/hr	63%	-
Gas Wall Gravity	over 27,000 up to 46,000 Btu/hr	64%	66%
Gas Wall Gravity	over 46,000 Btu/hr	65%	67%
Gas Wall Fan-Type	up to 42,000 Btu/hr	73%	75%
Gas Wall Fan-Type	over 42,000 Btu/hr	74%	76%

# Table 15: Minimum AFUE Requirements for Wall Furnacesmanufactured after January 1, 1990 and April 16, 2013

While thermal efficiency represents the full-load, steady-state performance of furnaces, AFUE is supposed to reflect furnace performance over a range of operating conditions. Many of the baseline furnaces in this study were manufactured before AFUE ratings were required. While all rated and tested AFUE values are reported, furnace efficiency comparisons rely mostly on thermal efficiency values.

Wall furnaces are located inside the building envelope, and all top vent furnaces use indoor air for combustion. This means that their performance tends to stay relatively constant under different weather conditions as compared to furnaces that sit in unconditioned or semi-conditioned spaces. It also means that laboratory-measured efficiencies should be fairly good job of predicting actual efficiency of wall furnaces as they operate in the field.

## **Related Emissions and Indoor Air Quality Guidelines**

Like all gas burning equipment, even properly operating wall furnaces produce low levels of CO, NOx, and particulate matter emissions. As with all primary gas space heating equipment in the state of California, emissions must be vented to the outside to prevent the accumulation of indoor pollutants.

There are no federal or California limits on flue gas emissions or indoor pollutants generated by wall furnaces. However, the Code of Federal Regulations limits particulate matter emissions from wood-burning residential forced-air furnaces. Residential forced-air furnaces are defined for this standard as fuel burning devices designed to burn wood or wood pellet fuel that warms a space other than the space where the furnace is located. Wall furnaces do not meet this definition because they burn natural gas, and because heat the space where they are installed.

For reference, forced-air furnaces manufactured after May 16, 2015 were required to emit no more than 0.93 lbm/MMBtu of particulate matter (CFR 60.5474 (b) (4) 2022), defined as the total of PM2.5 and PM10 particles. This limit was lowered to 0.15 lbm/MMBtu in total particulate matter for forced-air furnaces manufactured after May 15, 2020 (CFR 60.5474 (b) (6) 2022).

In California, the South Coast Air Quality Management District (SCAQMD) and the San Joaquin Valley Air Pollution Control District (SJVAPCD) limit NOx emissions from natural gas-fired fantype central furnaces distributed or sold in their territories. These standards do not specifically define a central furnace. It is typically a furnace that heats air in one place and circulates it through ducts to other places, so these rules do not apply to wall furnaces. For reference, both the SCAQMD Rule 1111 (SCAQMD 2021) and SJVAPCD Rule 4905 (SJVAPCD 2020) require furnaces to keep NOx emissions, on a basis of NO2, below 14 ng/Joule (0.033 lbm/MMBtu).

The US Environmental Protection Agency does not regulate indoor air quality, but they have characterized typical levels of carbon monoxide found in homes (US EPA CO 2022). They have not agreed upon standards for nitrogen oxides (US EPA NOx 2022) or particulate matter (US EPA PM 2022) within homes but have laid out acceptable levels for these pollutants in outside air over different time periods.

The US Environmental Protection Agency has developed guidelines for outdoor air quality, the National Ambient Air Quality Standards (US EPA NAAQS 2022), with acceptable limits of outdoor air pollutants in terms of averages over different time periods. The California Air Resources Board has also developed standards for outdoor air quality that are sometimes more stringent than federal standards, the California Ambient Air Quality Standards (CARB CO 2022, CARB NOX 2022, CARB PM 2022).

Table 16 summarizes the regulations, standards, and guidelines for residential furnaces and indoor air quality, as well as some outdoor air pollution standards. Although none of these standards applies to wall furnaces, they serve as reference values for this project's emissions and indoor air quality analyses. Note that no regulations, standards, or guidelines were identified that help characterize hydrocarbon emissions.

Rule	Equipment	CO	NOx	PM2.5 & PM10
Code of Federal Regulation	Residential forced-air furnaces, wood-burning	n/a	n/a	0.93 lbm/MMBtu, 2015 0.15 lbm/MMBtu, 2020
SCAQMD Rule 1111 & SJVAPCD Rule 4905	Central furnaces	n/a	0.033 lbm/MMBtu (14 nanograms/Joule)	n/a
US EPA reference levels of typical indoor air pollutants	Indoor air quality in homes	0 - 5 ppm normal 5 - 15 ppm near properly adjusted gas stove 30 ppm or more near improperly adjusted gas stoves	n/a	n/a
National Ambient Air Quality Standards	Outside air	9 ppm 8 hours 35 ppm 1 hour	100 ppb 1 hour 53 ppb 24 hours	PM2.5 35 ug/m <sup>3</sup> 24 hours PM10 150 ug/m <sup>3</sup> 24 hours
California Ambient Air Quality Standards	Outside air	9 ppm 8 hours 20 ppm 1 hour	180 ppb I hour 30 ppb 24 hours	PM2.5 none 24 hours PM10 50 ug/m3 24 hours

#### Table 16: Emissions and Indoor Air Quality Regulations, Standards and Guidelines

A-5